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ACOUSTIC LOCATOR SYSTEM: TEST RESULTS FOR THE UH-1 AND AH-1G

by

W. K. Stahlman
J. D. Hoopingarner
Operations Research, Inc.
1400 Spring Street
Silver Spring, MD 20910

and

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

Test results are presented for an airborne device called the Acoustic Locator System for detecting and locating the source of small arms fire directed at the UH-1 and AH-1G helicopters. The Acoustic Locator is considered usable on the UH-1, but not usable on the AH-1G.

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INTRODUCTION

The Acoustic Locator System is a device intended to detect and locate the source of small arms ground fire directed at Army helicopters. The system was first developed by Westinghouse Defense and Space Center under Contract DAADO5-67-C-0040 (Final Report titled: "Acoustic Locator System," Sept 67. AD 390885L) and then under Contract DAADO5-68-C-0227 (Final Report titled: "Improved Acoustic Locator System," Sept 69, AD 861-337L). The above two reports describe the development and operation of the systems. This report describes the tests of the Improved Acoustic Locator for the UH-1 and Cobra (AH-1G) aircraft.

In 1967, seven of the first Acoustic Locator Systems were evaluated in Vietnam by the Army Concept Team in Vietnam. The systems were found to be potentially useful but several improvements were suggested. These improvements were made and the resulting Improved Acoustic Locator Systems are discussed in this report. The Vietnam situation was changing and the Improved Acoustic Locator System was never evaluated in Vietnam. It was, however, tried on a Cobra, AH-1G, aircraft and found to be unsuitable for the Cobra aircraft because of the speed and noise level of the Cobra (Appendix B). In 1971, the improved Acoustic Locator System was evaluated by MASSTER, Ft Hood, Texas and the results are reported in MASSTER Report "Improved Acoustic Locator Systems Test Report, Volume II," March 72, AD 519864. In March 1974, the remaining pieces of the seven Improved Acoustic Locator Systems were transferred to the US Navy for use by the Los Angeles Police Department to evaluate their utility on police helicopters.

DESCRIPTION OF SYSTEM

The components of the Improved System are shown in Figure 1. The system weighs 41.5 lbs, occupies about 1.3 cu ft, and uses about 80 watts of electrical power at 28 VDC. In addition to the sensor pod, electronics box, and two displays shown in Figure 1, there are three interconnecting cables and various hardware used to mount these components to the two aircraft used.

A training device is also part of the equipment. This device provides simulated signals to a system while on the ground and allows operator training in interpretation of the display without the need for flying and firing.

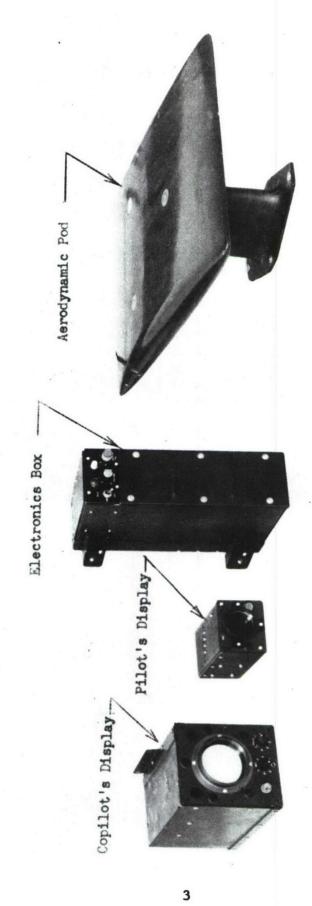


Figure 1. Improved Acoustic Locator System

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PRINCIPLES OF OPERATION

The Acoustic Locator System utilizes the acoustic signature generated by the firing of small-arms to detect and locate the source of small-arms fire directed toward the aircraft. The ballistic shock wave from the passing projectile is used to alert that fire is being received and then the direction of the arriving muzzle blast wave is used to indicate the direction to the source of fire. In addition to the direct waves, it is usually possible to receive a reflection of the ballistic shock wave from the ground.

In operation the system measures the transit time of the acoustic shock waves as they traverse three microphones mounted in the pad under the aircraft. The sequence in which these three microphones are traversed by a shock wave is related to the azimuth direction of the arriving wave. The time that it takes this shock front to traverse the three microphones is an indication of the depression angle of the wave. The Acoustic Locator System utilizes this information and displays the results on a PPI-type cathode ray tube display located in the pilot's and co-pilot's compartment of the aircraft. With this information the air crew can determine the direction of arrival of the shock front.

The Acoustic Locator System is not able to distinguish reliably between these two waves; hence, the system is designed to display the occurrence of both waves (and their reflections) and the judgement of the observer is used to distinguish between the two types of waves. Only the muzzle blast wave, which expands spherically about the weapon, provides the true direction to the source of fire.

TEST PROCEDURES AND RESULTS

Appendix A is the report of the contractor, Operations Research Inc., which describes the test design and the test results with the system mounted on a UH-1 aircraft. Appendix B describes a "check" test with the system mounted on an AH-1G. During both tests the operator of the system, flying in the co-pilot's seat, observed a single round fired from various types of weapons as the aircraft flew a clover leaf pattern centered over a fixed line of fire. The operator would then interpret the display, recording the azimuth and elevation to the weapons that he considered to be the source of the fire. The results of these tests for the various types of weapons, various miss distances, and various altitudes and speeds of the aircraft were then compiled and are reported in these reports.

CONCLUSIONS

- 1. The Acoustic Locator System experienced a higher-than-desired false-alarm rate. The false alarms were caused either by reflection of aircraft noises from the ground (when the aircraft is at low altitude) or by rotor "pops."
- 2. At speeds above 120 to 150 knots the noise of wind passing over the microphones increased to a level such that signals could not be detected at useful ranges.
- 3. The multiplicity of signals received from a single round (ballistic shock wave, sometimes the ballistic shock wave reflected from the ground, a muzzle blast and possibly a reflected muzzle blast) was confusing and required trained, experienced operators to operate the system. A training device was supplied with the systems to overcome this problem.
- 4. The detection of the source of ground fire directed at aircraft remains an operational problem. The US Army Land Warfare Laboratory has investigated both acoustic techniques and infrared techniques for detecting small arms and has found that both are range limited. Another approach which was not tried but which should be considered for future developments is a small, light-weight, airborne radar for detecting the bullet trajectory in the vicinity of the aircraft and a computer to determine the source of fire.

APPENDIX A

TEST AND ANALYSIS OF THE IMPROVED ACOUSTIC LOCATOR SYSTEM ABOARD THE UH-1



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Operations Research Incorporated

TEST AND ANALYSIS OF AN ACOUSTIC LOCATOR SYSTEM (U)

By W.K. Stahlman and J.D. Hoopingarner

September 1968

Declassified on 3 April 1974 by CDR, USALWL, APG, MD

(ORI Ref TR-517)

RICHARD L. CLARKSON

Colonel, AD Commanding

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PREFACE

The purpose of this work has been to obtain insights into the performance of an Acoustic Locator System prior to its employment in a tactical environment. The contents of this document consist of field test plans and the collected data from these tests. It is envisioned that this document would not be published as a separate report from the Limited War Laboratory, but would provide inputs to various reports to be subsequently published by the LWL. This effort comprises a portion (Work Assignment No. 6) of Contract No. DAAD05-68-C-0119, and consists of the design, monitoring and reporting results of the series of field tests of the equipment mentioned.

TABLE OF CONTENTS

			Page
	PREFACE		i
I.	INTRODUCTION	1	1
II.	DISCUSSION O	F TESTS	3
III.	PRESENTATION	OF DATA	10
	Factorial Te	sts	10
	False Alarms	S	25
	Instrumenta	tion Effects	25
	Azimuth Erro	or Bias	26
	Special Test	s	28
	Acceptance	Tests	33
	APPENDIX A	Listing of Test Data	
	Factorial Te	st Data	A-5
	Special Test	Data	A-22
	Acceptance	Test Data	A-30
	APPENDIX B	Test Plan dated 2 July 1968	
	APPENDIX C	Work Assignment	



(I. INTRODUCTION

- (U) The Army is developing an Acoustic Locator System (ALS) that is to be used aboard an aircraft for detecting the presence of ground fire directed at the aircraft and for locating the source of the fire in terms of azimuth and depression angles relative to the aircraft.
- The performance of the system is dependent upon the receipt of a bullet shock wave, a reflected bullet shock wave and a weapon muzzle blast. For this reason, an investigation of various factors which might affect this performance was conducted by a series of field tests at Aberdeen Proving Ground, Maryland. These tests provided information relevant to system performance while considering such factors as; weapon to aircraft range, bullet miss distance, aircraft altitude, aircraft speed, aircraft heading relative to the weapon position and type of weapon being used.
- (U) The contractor (ORI) was requested to (1) develop a test plan for evaluating the performance of the ALS, (2) monitor the implementation of the plan and, (3) reduce and analyze the resulting data from these tests.



- (U) Section 2. of this document, supported by Appendix B, discusses the tests conducted. Section 3. presents the data, in reduced form, from basic tests of the system along with a discussion of the special tests which were required and of the acceptance tests of the hardware of four additional Acoustic Locator Systems.
- (U) Appendix A is the computer listing of the raw data collected during the tests.
- (U) Appendix C is the work assignment which initiated this contractor effort.

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(X) II. DISCUSSION OF TESTS

(U) The test plan, dated 2 July 1968, is included as Appendix B to this report. The conduct of the tests was as outlined in the plan. The plan called for "blocks" of tests to be conducted—each block at a given range and bullet miss distance with altitude, speed, azimuth, and weapon type varied within each block. The blocks of tests were to be conducted in an order best satisfying a priority scheme developed by the test director in order that limitations of time and resources would impose a minimum penalty on the ALS test program.

Range Miss Dist. Ft.	500	750	1000	1200	1400	1600
100 Ft.						
200 Ft.		2 Aug	5 Aug	7 Aug	8 Aug	
300 Ft.	7 Aug	5 Aug	8 Aug	2 Aug		

FIGURE 1; TEST BLOCKS

3



- (K) The above figure represents the program blocks of tests which were considered as feasible. Because of time limitations, only 8 blocks were run. The dates on which each of these blocks was conducted indicates the priority established for conduct of the tests. As can be seen, 100 foot miss distances and 1600 ft. ranges were assigned a lower priority and subsequently were not a part of the basic test program. The 8 highest priority blocks of tests were conducted and provide valuable data for performance evaluation of the ALS.
- (C) As a further means of meeting time and range limitations, the test design allowed for the program within each test block to be changed if necessary. The 15 and 1000 ft test altitudes were eliminated during the basic tests. In addition, the planned aircraft speed of 0 knots was changed to 20 knots when it became apparent that the hover speed over the range marker was somewhat difficult to maintain.
- (C) The basic test plan was a factorial test design to include six factors considered to have most effect on system performance and was the means for providing the basic statistical information on the overall system performance.
 - (U) Special tests were conducted for two purposes:
 - To demonstrate system performance in terms of additional levels of the six basic factors, and
 - b. To demonstrate system performance in terms of additional factors.
 - (€) A total of eight special tests were conducted as follows:



Special Test No. 1

Data from this test have been designated as test M. The purpose of the test was to investigate levels of altitude in addition to those levels used in the factorial tests. This group of tests were all conducted using a range of 500 ft., a miss distance of 300 ft., a speed of 20 knots and using the M14 weapon. One run (4 tests) were conducted at each of eight altitude steps: 25, 50, 75, 100, 150, 200, 300 and 500 feet. These 32 tests were conducted on August 8, 1968.

Special Test No. 2

The purpose of this test was to investigate the performance of the system when fire from more than one source was being directed toward the aircraft. A 50 caliber MG was located such that the range would be 500 feet and the miss distance 100 feet. The M60 was located such that the range was 500 feet and the miss distance 300 feet with the bullet path located on the opposite side of the aircraft from the 50 cal. bullet path. Two cloverleaf patterns were run, each with the aircraft at 200 ft. altitude and 80 knots speed. During the first run, each weapon fired a single round and during the second run, each weapon fired a five round burst. These 8 tests were conducted on August 8, 1968 and data from these tests are referred to as being test N in this document.



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Special Test No. 3

These tests were conducted on August 13, 1968 for the purpose of investigating additional levels of range and speed, additional weapons, and the rapid fire of the weapons. There were 120 tests in this group, all except 12 were conducted at 80 knots. These 12 were conducted at 100 knots. Ranges were 1000, 1200, and 1400 feet with miss distance of 100 and 200 feet. Various weapons were fired during these tests. The weapons included the M1, M16, M14, M60 50 cal., AK56, 7.62, 12.5, 20 mm, and the 23 mm. Data from these tests are designated as test O in this document.

Special Test No. 4

On August 8, 1968, eight tests were conducted in an attempt to evaluate system performance for detecting ground fire while return fire is being generated from the aircraft. This situation was performed at 500 ft. range, 200 foot miss distance, 200 foot aircraft altitude and 40 knots speed. The M14 was fired from the ground position while return fire was from the M60 located inside the aircraft.

Special Test No. 5

Eight tests were conducted on August 9, 1968 for the purpose of investigating system performance with the aircraft loaded with additional weight.

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It was expected that increased aircraft weight might cause additional rotor pops which would be picked up by the system as false alarms thereby readjusting the system threshold levels. An additional 1400# of weight were in the aircraft. Other parameter levels included; range, 500 feet; miss distance 200 feet; speed 80 knots; altitude 200 feet; and weapon M14. Data from these tests are noted as test Q in this document.

Special Test No. 6

The basic test program was conducted so that the path of a passing bullet was theoretically in the same horizontal plane as the aircraft. On August 9, 1968, 16 tests were conducted where the bullet path was higher than the aircraft indicating a specific miss direction. The levels of the parameters which remained constant for these tests were; range 500 feet, altitude 200 feet, and speed 20 knots. Aircraft headings were 90° and 270° only indicating fire from aft and in front of the aircraft. Although the weapons were positioned at the normal 100 foot miss distance position, the elevation angles of the weapons were adjusted so as to provide a miss distance of 200 feet for 8 tests and 300 feet for the other eight tests. Weapons used were the 50 caliber for eight tests and the M60 for the other eight tests. Data from these tests are referred to as test R in this document.

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Special Test No. 8

For this group of tests, the system was installed in a UH-1B helicopter as opposed to the UH-1D helicopter used for the majority of the other tests. A normal block of tests was run with the exception of the 40 knot speed, the 750 ft. range, the 1000 range-200 miss distance, 2300 ft. range-200 ft. miss distance, the 1400 ft. range and the M16 weapon. On August 16, 1968, a total of 104 tests were conducted for the expressed purpose. Data from these tests are referred to in this document as test T.

- (U) The above tests did not include 96 tests conducted on August 19, 1968 with the same plan but with a portion of the instrumentation being disconnected. Restuls of these 96 tests are referred to as Test U in this document.
- (S) Acceptance tests were conducted for four additional ALS. System one was tested on August 22, system two and three on August 26 and system four on August 27. A total of 96 tests were conducted on each of the four systems. These tests provided an investigation of all the levels of parameters investigated during the factorial tests with the following exceptions.
 - (a) 750 and 1400 feet range
 - (b) 200 ft. miss distance at 1000 and 1200 ft. range
 - (c) 40 knot speed at all ranges
 - (d) M16 weapon at all ranges.

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This, in effect, resulted in the same test plan used in special test 8.

(U) Minor modifications were provided for in the flexible test plan and the net result of the total program reflects a reasonable test plan, good implementation of the plan, and the collection of valuable data describing the performance of the ALS.

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(C) III. PRESENTATION OF DATA

(U) This section is divided into three parts as inferred in Section 1. The attempt has been to present only the basic test results in a reduced form. Computer listings of the test data appear in Appendix A. These data were placed on punch cards which easily allowed for the necessary sorting and listing to be done to facilitate this effort. Additional sorts can easily be made to produce additional combinations of factors for any desired analysis at a later time.

Part 1. Factorial Tests

(C) Data from these tests include all combinations of the test parameters listed below with exception of the 500 ft range 200 ft miss distance and the 1400 ft range 300 ft miss distance.

Range - 500, 750, 1000, 1200, 1400 ft.

Miss Distance - 200 and 300 ft.

Aircraft Altitude - 50, 200 and 500 ft.

Aircraft Speed - 20, 40 and 80 knots

Aircraft Heading - 0, 90, 180 and 270 degrees

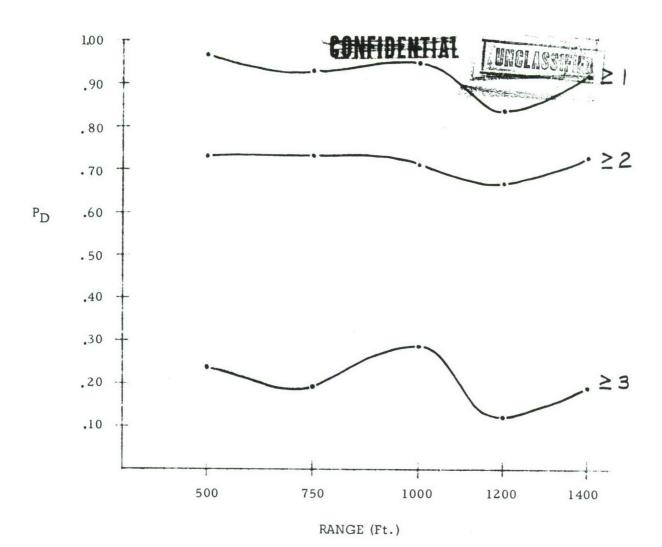
Weapons fired - M-16, M-14 and 50 cal MG



- (4) Figure 2. shows the probability of receiving a certain number of signals at each of the ranges. The mean of the five values of the upper curve is .92 which represents the overall probability of detection for the test conditions.
- (U) Figure 3. reveals how each of the test parameters affected the probability of detection. All the curves in Figure 3. are based on probability of detection being defined as the receipt of one or more of the signals.
- (U)Figure 4. shows the relative frequency of azimuth errors being as specified in the bounds as noted in the graph legend.
- (U) Figure 5. shows the effect of each test parameter on the azimuth error at each of the various test ranges.
- Figure 6. reveals the effect of each of the test parameters on those cases where the azimuth error was less than 7.5°. This value was chosen as a reasonable value for resolution of reading the display.

 Azimuth error is defined as the absolute difference between the recorded angle and the calculated angle.
- (U)Figure 8. indicates the relative frequency of the depression error being within certain bounds. Figure 9. reveals the effect of each of the test parameters on the depression angle error.
- Figure 10. indicates the depression angle error as a function of the calculated depression angle. This shows a decrease in reading error with an increase in the calculated depression angle. This can be accounted for since the display is such that the accuracy of reading larger depression angles is inherently better than for reading smaller angles.



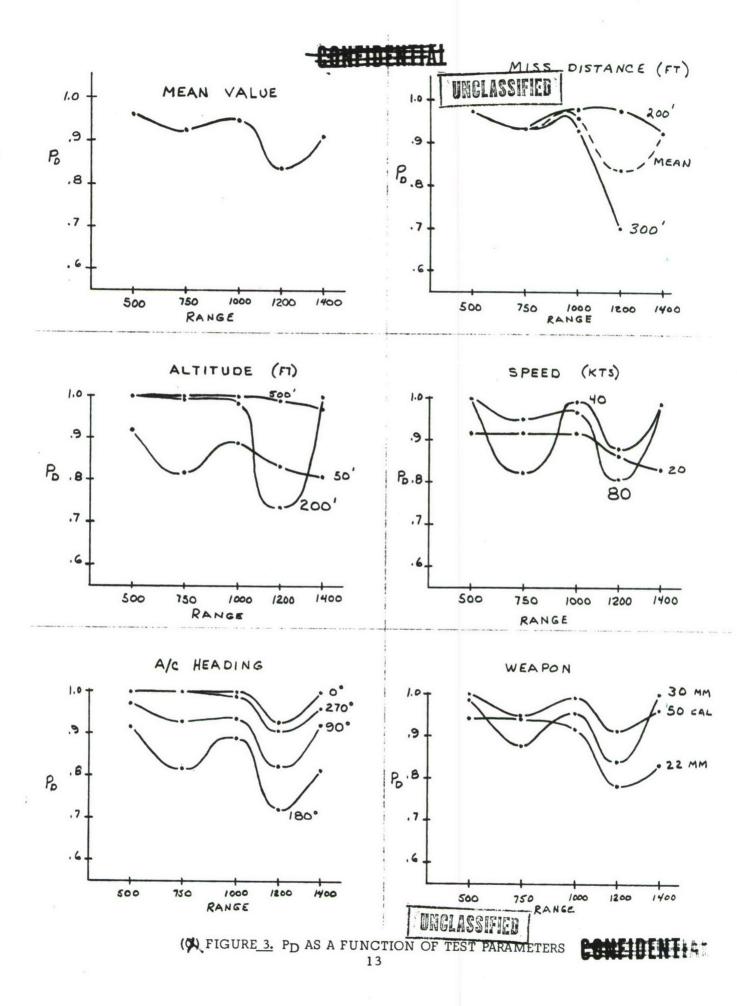


Signals			RANGE (F	't.)		TO THE
Received	500	750	1000	1200	1400	TOTAL
None	3	14	10	32	8	67
3 or More	26	43	63	25	21	178
2 or More	79	159	143	137	79	507
l or More	105	202	206	172	100	785
TOTAL	108	216	216	204	108	852

(FIGURE 2. PROBABILITY OF DETECTION





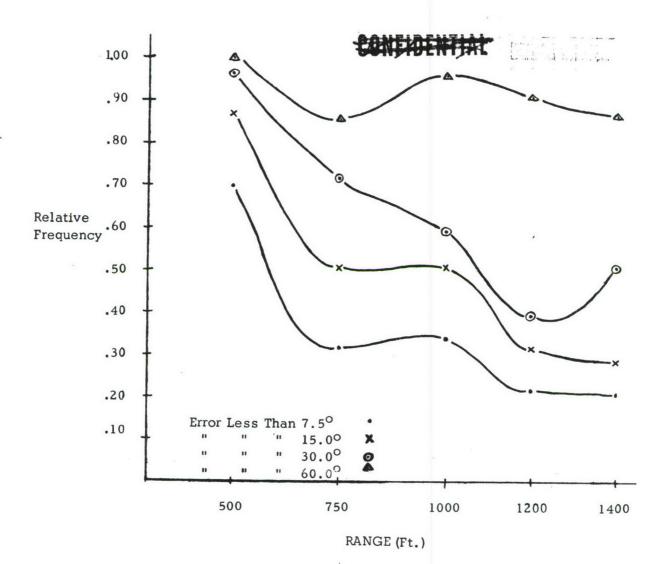


				RANGE (Ft.)			of the community of the state o	TOTALS	
		500	750	1000	1200	1400	Z	×	PD
Miss	200	X	7-108	3-108	3-108	8-108	432	21	.951
Distance	300	3-108	7-108	7-108	29-96	X	420	46	068.
D/C	50	3-36	13-72	8-72	12-72	7-36	288	43	.851
Altitude	200	0-36	1-72	2-72	19-72	0-36	288	22	. 924
	200	0-36	0-72	0-72	1-60	1-36	276	2	.993
	20	3-36	6-72	6-72	10-72	6-36	288	31	.892
A/C	40	0-36	5-84	1-72	8-60	1-36	288	15	. 948
peed	80	0-36	3-60	3-72	14-72	1-36	276	21	. 924
	06	1-27	4-54	3-54	9-51	2-27	213	19	.911
A/C	180	2-27	10-54	6-54	14-51	5-27	213	37	.826
ding	270	0-27	0-54	1-54	5-51	1-27	213	7	196.
	0	0-27	0-54	0-54	4-51	0-27	213	4	. 981
	22	2-36	4-72	6-72	15-68	6-36	284	33	.884
Weapon	30	1-36	7-72	3-72	11-68	0-36	284	22	. 923
	20	0-36	3-72	1-72	89-9	2-36	284	12	. 958
	Z	108	216	216	204	108		852	
TOTAL	×	3	14	10	32	8		29	
	PD	.972	.935	.954	.843	.926		.920	

N = Number of Tests ConductedX = Number of Tests Where No Signal Was Received

(\$\pi\$) FIGURE 3. (Cont.) PD AS A FUNCTION OF TEST PARAMETERS s-t indicates of t tests conducted, s tests provided no signal

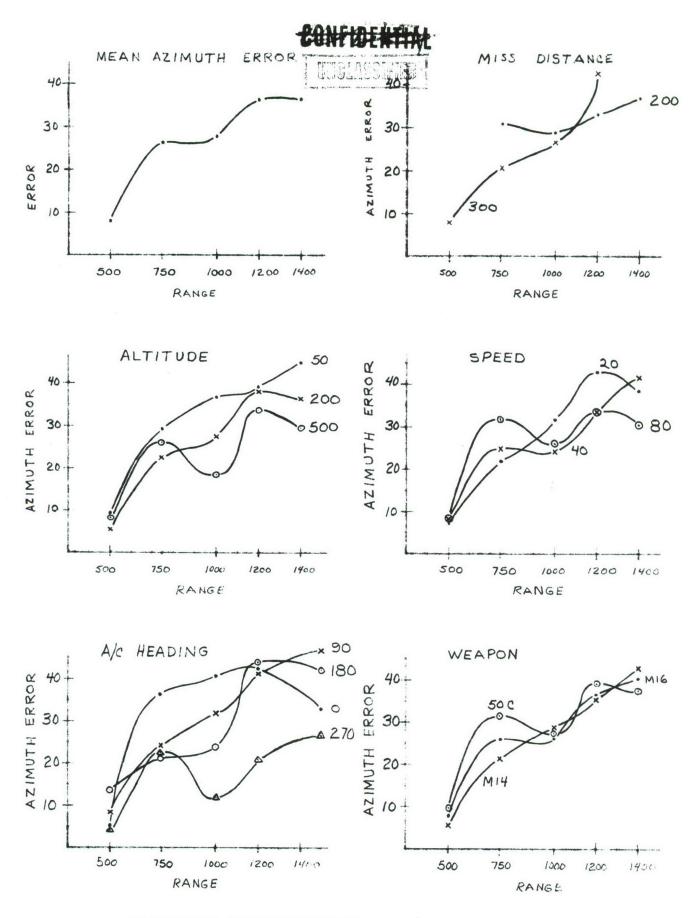




Number of detections			RANGE	(Ft.)	
with azimuth error	500	750	1000	1200	1400
less than 7.50	73	64	71	38	21
less than 15.00	91	102	106	55	28
less than 30°	101	146	122	68	51
less than 60°	105	173	199	155	87
Total Detections	105	202	206	172	100

($\not x$) Figure $\underline{4}$. Frequency of Azimuth Error





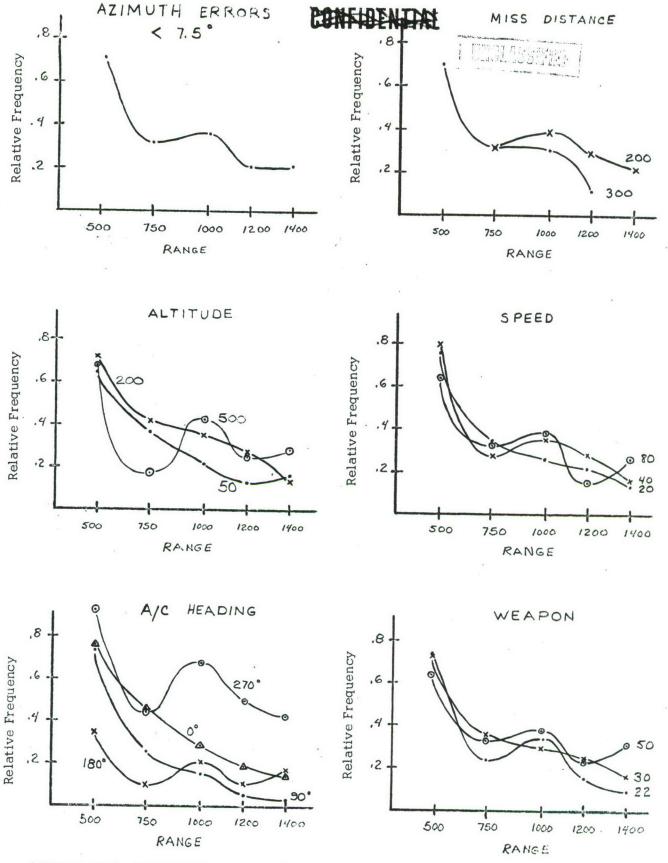
(5) FIGURE 5. AZIMUTH ERROR AS A FUNCTION OF TEST PARAMETERS



RANGE	GE	5	200	7	750	10	1000	17	1200	1,	1400	TOI	TOTALS
/		Z	п	N	π	N	п	Z	п	Z	π	N	η
Miss Distance	200	X E	χ .	66	30.7	105	28.2	103	33.6	ο χ	36.7 X	407	32.2
	2		2		2.13		1.07	0	75.3			900	66.3
	90	31	9.4	55	29.5	63	36.7	58	39.2	29	45.0	236	33.1
A/C	200	36	5.7	71	22.8	20	27.3	52	38.2	36	36.7	265	9.92
Altitude	500	36	8.7	72	26.0	72	18.6	59	34.2	35	29.8	274	24.0
	20	31	7.8	63	21.8	99	31.4	62	43.1	30	38.5	252	29.8
A/C	40	36	7.9	62	25.0	20	24.4	20	33.4	35	41.5	270	30.0
Speed	80	36	7.8	99	31.7	69	26.0	57	33.8	35	30.4	253	27.0
						I							
	0	56	5.5	54	36.4	54	40.2	47	45.5	27	33.0	208	34.4
D/V	90	25	8.2	49	24.6	90	31.8	41	41.1	25	46.3	190	30.8
Heading	180	25	13.4	43	20.8	48	23.6	38	44.6	22	42.0	176	28.3
	270	27	4.7	53	21.8	53	11.8	44	21.0	97	26.7	203	17.4
	M16	33	7.7	99	25.4	99	25.6	53	36.2	30	40.2	248	27.2
Weapon	M14	34	5.9	64	21.4	69	28.6	56	35.8	36	42.7	259	27.4
4	20G	36	8.6	69	31.4	20	26.6	61	39.0	34	27.2	270	28.5
POTATO	Z	103	X	198	X	205	X	169	X	100	X	775	\bigvee
LOINES	п	X	7.8	X	97	X	27.2	X	36.2	X	36.7	X	27.5
	M - M	mhor	N = Number of Toots	200	7.0400								

N = Number of Tests Conducted $\mu = Mean Azimuth Error (Degrees)$

(\$) FIGURE 5. (Cont.) AZIMUTH ERROR AS A FUNCTION OF TEST PARAMETERS



(C) FIGURE 6. FREQUENCY OF <7.5° AZIMUTH ERRORS AS A FUNCTION OF TEST PARAMETERS

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				RANGE (Ft.)	-			TOTALS	
		200	750	1000	1200	1400	N	×	Rel. Freg.
Miss	200	X	32-101	40-105	31-105	21-100	411	124	.302
Distance	300	73-105	32-101	31-101	79-7	X	374	143	.382
	50	22-33	22-59	14-64	8-60	5-29	245	7.1	.290
A/C	200	26-36	29-71	25-70	15-53	5-36	992	100	.266
Altitude	200	25-36	13-72	31-72	15-59	10-35	274	94	.343
	20	23-30	23-36	18-66	14-62	4-30	224	82	.366
A/C	40	27-36	22-79	25-71	15-52	6-35	273	96	.348
Speed	80	23-36	19-57	27-69	9-58	10-35	255	88	.345
	06	19-26	13-50	8-51	2-42	1-25	194	43	.222
A/C	180	9-25	2-44	10-48	4-37	4-22	176	53	.165
Heading	270	25-27	24-54	36-53	23-46	11-26	902	119	.578
	0	20-27	25-54	16-54	9-47	4-27	509	74	.354
	22	25-34	17-78	22-66	8-53	3-30	261	75	.288
Weanon	30	25-35	24-65	2.1-69	15-57	96-36	292	91	.347
	20	23-36	22-69	27-71	15-62	11-36	274	86	.358
	Z	105	202	206	172	100		785	
TOTAL	×	73	64	71	38	21		267	
	Kel. Freq.	.70	.32	.34	.22	.21		.34	

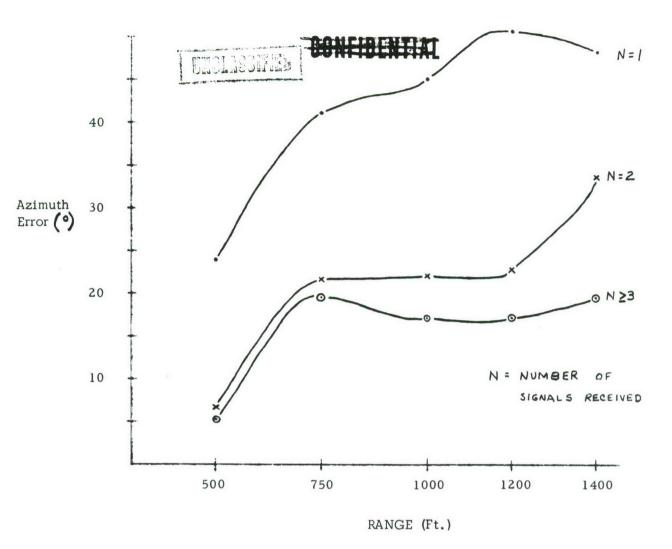
N = Number of Tests Conducted

 $X = Number of Tests With Error < 7.5^{O}$

s-t indicates of t tests conducted, s tests provided azimuth errors less than 7.5 $^{\rm O}$

(*) FIGURE 6. (Cont.) FREQUENCY OF <7.50 AZIMUTH ERROR AS A FUNCTION OF TEST PARAMETERS

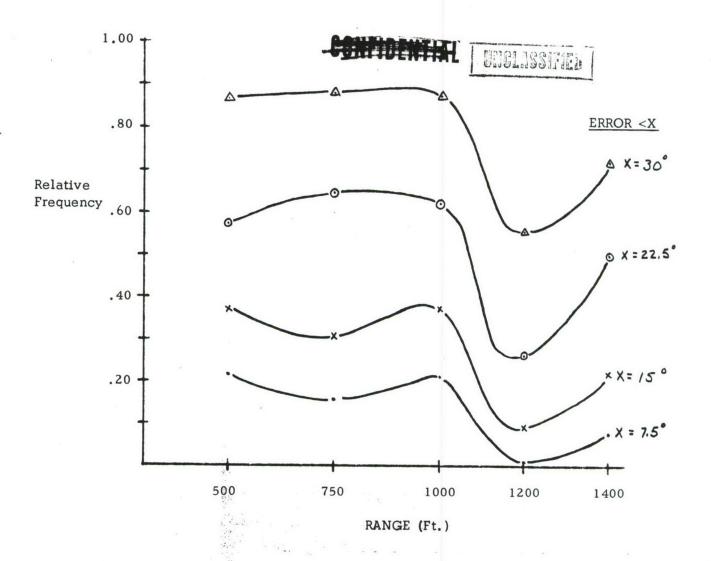
unglassifie.



No. Range(Ft)	5	00	7	50	100	00	12	00	14	00
of Signals Received	N	¥	N	μ	N	μ	N	μ	N	μ
1	10	24	46	41.3	58	45.2	90	51.3	42	48.2
2	67	6.5	112	21.7	83	22.0	55	22.9	37	33.6
≥3	26	5.3	42	19.4	64	17.0	25	17.1	21	19.0

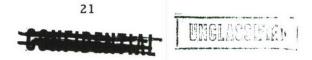
N = Number of Tests $\mu = Mean Azimuth Error$

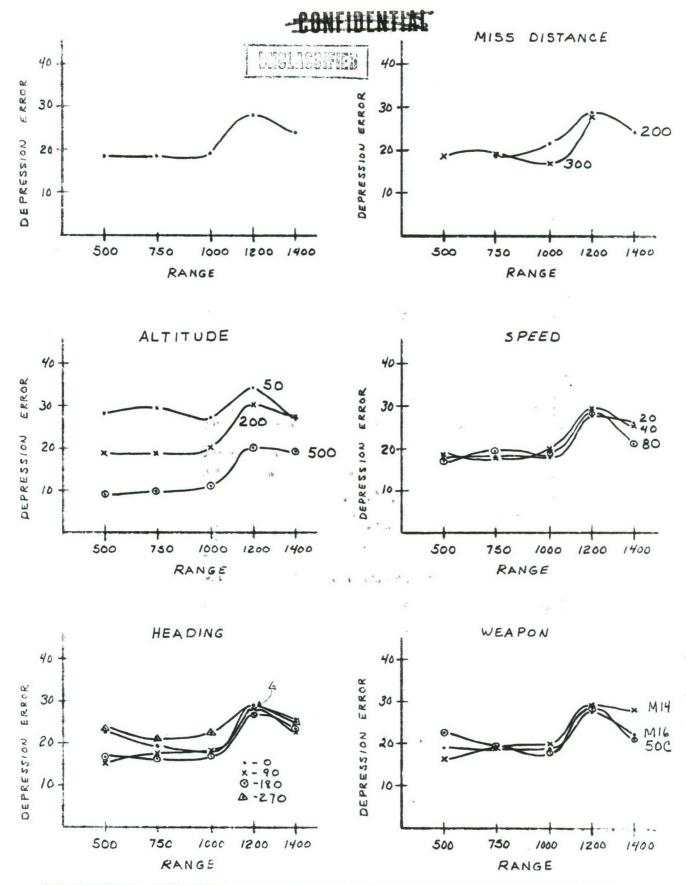
(C) FIGURE 7. AZIMUTH ERROR BY NUMBER OF SIGNALS RECEIVED



Range	5	00 ft.		750 ft.		1000 ft.	1	200 ft.	1	400 ft.
Error Less Than	N	Rel. Freq.								
7.5	22	.21	30	.15	42	.21	1	.07	8	.08
15.0	38	.37	60	.30	76	.37	15	.09	22	.22
22.5	59	.57	128	.64	127	.62	43	.26	50	.50
30.0	94	.90	175	.87	180	.87	93	.55	72	.72
Total Readings	104	Week Art 1	200	Scarne Caldin	206		168	the abit.	100	

FIGURE 8. FREQUENCY OF DEPRESSION ANGLE ERRORS





(C) FIGURE 9. DEPRESSION ANGLE ERRORS AS A FUNCTION OF TEST PARAMETERS

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		5	500	7	750	1	1000		1200	14	1400		
		N	η	z	ח	Z	п	Z	7	z	77	IN	3 .
Miss	200	X	X	101	18.3	105	21.2	103	28.4	100	24.1	409	23.0
Distance	300	104	18.0	66	18.7	101	17.0	99	27.9	X	X	370	19.7
	20	36	8.9	57	2.62	64	27.0	58	34.4	29	26.6	244	26.6
A/C	200	36	18.5	71	18.8	20	20.4	52	30.2	36	26.8	592	22.5
Altitude	200	32	27.9	72	6.6	69	19.1	59	20.4	35	19.3	270	15.9
	20	32	17.8	64	18.3	99	17.8	62	27.6	30	25.9	254	21.3
A/C	40	36	18.7	42	18.0	71	20.4	49	2.6.2	35	25.4	270	21.8
Speed	80	36	17.6	57	19.4	69	19.1	58	27.8	35	21.4	255	21.2
	0	27	22.3	54	19.1	54	17.6	46	2.62	27	25.3	208	22.2
5/0	06	25	15.6	49	17.7	51	18.2	41	28.2	25	22.8	191	20.5
Heading	180	25	16.4	43	16.4	48	17.4	38	26.9	22	23.3	176	19.8
	270	27	22.4	54	20.4	53	22.4	45	28.3	56	25.0	205	23.5
	22	34	18.8	29	18.3	99	18.6	54	27.5	30	22.3	251	20.9
Woapon	30	34	16.4	64	18.2	69	20.0	55	29.5	36	27.9	258	22.1
vea poi	20	36	22.4	69	18.9	71	18.4	61	28.0	34	21.6	271	21.6
TN		104	X	200	X	2.06	X	169	X	100	X	770	X
ח			18.0	X	18.5	X	19 2	X	28 2	T	1 7 7 7	X	1
					600		7117		77.07		7.4.		21.4

N = Number of Testsu = Mean Depression Angle Error

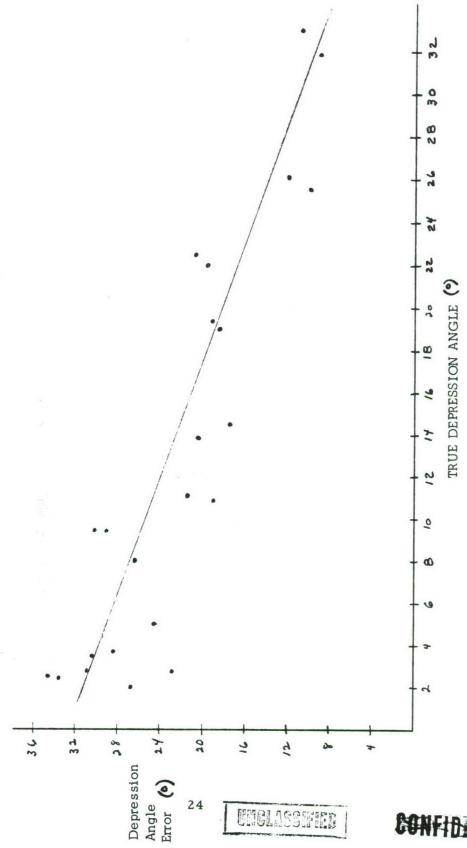
(#) FIGURE 9. (Cont.) DEPRESSION ANGLE ERRORS AS A FUNCTION OF TEST PARAMETERS

23





Unclassified



(C) FIGURE 10. DEPRESSION ANGLE VRS ANGLE ERROR

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False Alarms

In addition to the data presented in the graphs, charts and computer listings, an analysis of the false alarms was made in an attempt to define the conditions generating these alarms. During the total of approximately 860 tests, false alarms were indicated on the data forms for a total of 121 of these tests. The number of false alarms per test varied from 1 to 5 with a reported total of 196. Of the six basic factors investigated, it would appear as if changes in altitude and speed would most likely influence the false alarm rate. A further look at the 196 false alarms reveals they were divided in the three altitude and speed categories as noted below.

Altitude	False Alarms	Speed	False Alarms
50	98	20	35
200	52	40	111
500	47	80	50
	196	Marie - 1980 (Britania - Marie Britania - Marie Antonio Antonio Antonio Antonio Antonio Antonio Antonio Antonio	196

(FIGURE 11. FALSE ALARM ANALYSIS

Instrumentation Effects

During the conduct of the tests, it became apparent that switching off and on of the power to the recording instrumentation would generate false alarms. Some tests were conducted in an attempt to define the extent of the instrumentations effect upon the performance of the ALS. The hypothesis was that the recorder feedback was causing the threshold level to be maintained at a higher point than it would normally be thus causing fewer false alarms and possibly a lower detection rate than would be experienced by the system without the recording instrumentation attached. The series





of tests disignated special tests T were chosen for a comparison since the plan of the tests with instrumentation disconnected was a repeat of the plan for the tests of group T. These tests with the instrumentation disconnected are designated as test U for this description.

	Test T	Test U	All Fac- torial Tests
Probability of receiving			
l or more signals	1.00	.98	.92
2 or more signals	.69	.64	.60
3 or more signals	.19	.21	.21
4 or more signals	.03	.04	?
Number of False Alarms	5	106+*	196

^{*} In addition some reports of false alarms merely indicated "many".

FIGURE 12. INSTRUMENTATION EFFECTS ON ALS PERFORMANCE

Azimuth Error Bias

(c) The test design was such that azimuth reading errors would tend to be biased in the clockwise direction. This is primarily due to the fact that azimuth readings based on a signal other than the muzzle blast would always represent an azimuth error in the clockwise direction. A significant number of these situations were apparent in the tests. Test results are shown below:



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No. of cases at Heading the given a/c heading when	90 ⁰	180°	270°	00
Reading was clockwise from true azimuth	169	163	129	93
Reading was identical to true azimuth	7	2	16	8
Reading was counter- clockwise from true azimuth	14	11 .	58	106

FIGURE 13. BIAS OF AZIMUTH ERROR AS A FUNCTION OF AIRCRAFT HEADING

Range (Ft.) No. of cases at given range when	500	750	1000	1 200	1400
Reading was clockwise from true azimuth	55	111	156	137	93
Reading was counter- clockwise from true azimuth	48	53	49	33	6

FIGURE 14. BIAS OF AZIMUTH ERRORS AS A FUNCTION OF RANGE



Part 2. Special Tests

(U) As stated in Section 1, special tests were run as demonstrations of the system under conditions other than those conducted in the basic tests. Replications during these demonstrations were limited to the extent that statistical significance of variations in values is difficult to establish. Figure 15 presents the results of each of the special tests along with a value received from the test of similar conditions during the basic test program. Raw data from the special tests appear in Appendix A and can be distinguished by the letter (M through T) appearing in column one of the computer listings.

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							糙		H	H	ŧ		1 : 17	175		30		13	1			
	FT	. 26.6	1			22.5	15.9		20.9		21.6		-		-	-		-	21.3	21.8	21.2	- 1
ΔD	ST	19.8	41.2	•	21.0	14.8	10.8	d.	22.3	26.0	17.3	13.4	30.8	23.7	15.5	24.8	15.2	15.2			20.5	29.1
A	FT	33.1	-	!	!	9.92	24.0	distinguishable. signals were presented.	27.1	27.4	28.5		-	!	-				29.8	30.0	27.0	!
AA	ST	35.5 13.2	23.0		13.2	7.8	7.2	each signal was distinguishable.	48.5	27.6	83.0	21.2	8.89	92.6	38.2	45.6	0.06	132.0		1	53.5	27.8
PD	FT	. 85	!	!	!	.92	66.	was dist of sign	. 884	.923	.958		!	!	!	1	-		.892	.948	.924	
4	ST	1.0				_	1.0	signal was	88	1.00	1.00	1.00	1.00	.88	1.00	1.00	1.00	1.00	-	-	86.	1.00
Tests	FT	0 288	0	0	0	288	276	per weapon, each from each weapon,	284	284	284	0	0	0	0	0	0	0	288	288	270	0
No. of	ST	4			-		▶ 4	per wear	80	28	91	80	12	12	12	12	4	4	0	0	108	12
D	rarameter	25'	75'	100'	150	200	300' 500'	With one round per weapon, With rapid fire from each we	M16	M14	50C	M1	M60	AK56	7.62	12.5MM	20 MM	23 MM	20 Kts	40 Kts	80 Kts	100 Kts
Purpose of	Special Test	Investigate additional levels of altitude						Multiple firings	Investigate the use	of additional weapons									Investigate additional	a/c speeds		
Special	Test	M-1	:					N-2							0-3							

SPECIAL TEST RESULTS (K) FIGURE 15.



			CON	HANTENT UNC	Lassifieb
Q	FT		18.0 19.7 22.5 21.2 20.5 20.5 19.8 23.5 22.2 22.2	19.2 22.5 21.3 20.5 23.5 23.5	18.0 19.2 28.2 19.7 26.6 22.5 21.3
Δ	ST		8.88 8.88 8.7.7 15.0 8.8	15.7 15.7 15.7 15.7 18.7 14.0	15.0 18.8 18.8 17.5 20.5 14.9 18.7
A	FT		7.8 22.5 26.6 27.0 30.8 28.3 17.4 34.4	27.2 26.6 29.8 30.8 17.4 28.5	7.8 27.2 36.2 22.5 22.5 33.1 26.6 29.8
٥	ST	lable.	9.1 9.1 9.1 9.5 10.5 12.0	7.7 7.7 7.7 7.7 11.5 5.8 5.8	12.9 27.9 49.2 29.8 34.0 26.0 28.7
PD	FT	sis avai	. 972 . 890 . 924 . 911 . 911 . 967 . 981	. 954 . 924 . 892 . 911 . 967	. 972 . 954 . 843 . 890 . 851 . 924 . 892
	ST	no analysis available	1.00	. 69 . 69 . 69 . 38 . 38	. 97 1.00 . 98 . 98 . 97 1.00
of Tests	FT	data	108 420 288 276 213 213 213 213	216 0 288 288 213 213 284	108 216 216 420 288 288 288 276
	ST	Sparse	0 0 0 0 0 N N N N 0	, 16 16 16 16 8 8 8	68 68 64 200 96 104 96
Parameter		·	500 RANGE 300 Miss Distance 200 Altitude 80 Speed 90 180 270 M14 weapon	1000 Range 100 Miss Distance 200 Altitude 20 Speed 90 Heading 270 Meading M60	500 1000 1200 300 Miss Distance 500 200 80 Speed
Purpose of	Special Test	Investigate Perfor- mance with firing from a/c weapons	Use of system with a aircraft loaded with an additional 1400 lbs.	Firing <u>over</u> the a/c	Use of UH-1B Helicopter
Special	Test	P-4	Q-5	R-6	FI -8

(%) FIGURE 15, (Cont) SPECIAL TEST RESULTS

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RESULTS
PECIAL TEST F
(Cont)
FIGURE 15.
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								=	1	H		7	115				JMI		13	31;		
D	FT	20.5	19.8		22.1	21.6		18.0	19.2	28.2	19.7		26.6		21.3	•	0.5	19.8	23.5	22.2	22.1	21.6
٥	ST	17.5	18.0			•	11.2	15.1	18.9	20.02	18.0		20.9		18.6	C • 11	18.0	19.9		14.6	18.6	17.5
A	FT	30,8	28.3	34.4		28.5		7.8	27.2	36.2	22.5		33.1		29.8	0.17		28.3	17.4	34.4	27.4	28.5
٥	ST	31.9	28.4	36.3			46.5	7.0	19.7	41.8	23.2		26.8		24.8		38.2	19.4		16.3	25.1	21.4
-	FT	.911	.826	.981	.923	.958		.972	.954	.843	.890		.851		268.	+76.	.911	.826	196.	.981	.923	.958
Pn	ST	.98	86.	1.00	.97	1.00	1.00	.94	1.00	1.00	86.		96.		96.	1.00	96.	1.00	96.	1.00	96.	1.00
f Tests		213	213	213	284	284		108	216	216	420		288		288	0/7	213	213	213	213	284	284
No. of		50	50	20	96	96	4 4	32	32	32	96	r	48	2	48	40	24	24	24	24	48	48
	Parameter		Heading			Weapon			Range		Miss	Distance	Altitude			peed		Hoading			TAT	wedpon
	Pa	606	180	270	M147	20C	AK56 AK47	200	1000	1200	300		50	200	20	08	06	180	270	0	M14	50C
Pirrose of	Special Test							Instrumentation	Partially	Disconnected												
Special	Test	T-8 (Cont)																				

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ST indicates Special Test NOTE:

FT indicates Factorial Test

PD indicates probability of detection - at least one signal received

 ΔA indicates the difference between the absolute mean of the azimuth readings for a given test and the calculated azimuth 4.

 ΔD indicates the difference between the absolute mean of the depression readings for a given test and the calculated depression 5

See explanation on page 7. 9

(4) FIGURE 15. (Cont) SPECIAL TEST RESULTS

CONFLICTION

Part 3. Acceptance Tests

(U) In addition to the hardware of the ALS tested during the basic tests, it was necessary to obtain some indication as to the performance of the hardware to be used in four additional ALS. The hardware referred to consist of four basic elements for each system. These elements are the sensor housing, an aerodynamic pod, which is externally mounted on the aircraft and contains the transducers, an electronic processing unit mounted inside the aircraft and two display units, one located for the pilot observation, the second for co-pilot observation.

(U) Data forms from the tests indicate each of the different elements used was assigned a particular number and the total system under test was comprised of the numbered elements as designated in Figure 16.

System being tested	Sensor housing number	Electronic processing unit number	Pilot display unit	Co-pilot display unit
1	7	. 7	6	6
2	5	6	1	2
3	3	4	7	4
4	4	5	5	5

(U) FIGURE 16. ELEMENTS OF EACH SYSTEM

(U) The raw data from these tests appear in Appendix A with a recap as shown in Figure 17. The mean values obtained from similar runs during the factorial testing appear in Figure 17 for comparison.

EDITION THE



Rais		PD	D		AZ	AZIMUTH ERROR	H ERR	JR	DEP	DEPRESSION ERROR	N ERR		NUM	NUMBER OF TESTS	TESTS	50
JEMICE.	500	1000		1200 Total		1000	1200	500 1000 1200 Total 500 1000 1200 Total	500	1000	1200	Total	200	500 1000 1200 Total	1200	Total
Factoral Test Mean Values	. 97	. 95	. 84	26.	7.8	27.2	36.2	27.5	18.0	19.2	28.2	7.8 27.2 36.2 27.5 18.0 19.2 28.2 21.4 108		216	216	864
System #1	. 94	. 94	.97	56.	11.6	30.0	32.5	.95 11.6 30.0 32.5 25.8 16.5 20.8 22.8 20.0	16.5	20.8	22.8	20.0	32	32	32	96
System #2	1.00	. 91	. 95		25.3	32.8	47.7	33.2	19.5	22.8	24.6	.95 25.3 32.8 47.7 33.2 19.5 22.8 24.6 22.0 32	32	32	20	84
System #3*	. 88	. 78	. 81	. 82	16.5	33.4	46.8	.82 16.5 33.4 46.8 31.8 21.3 24.4 30.8 25.5	21.3	24.4	30.8	25.5	32	32	32	96
System #4	. 94	. 94	. 88	. 92	12.8	31.6	40.9	.92 12.8 31.6 40.9 28.4 16.3 25.8 24.9 22.2	16.3	25.8	24.9	22.2	32	32	32	96

Azimuth and depression error values are degrees. NOTE: P_{D} is based on the receipt of at least one signal

(Ç) FIGURE 17. ACCEPTANCE TESTS RESULTS

(C) APPENDIX A LISTING OF TEST DATA



APPENDIX A

The data appearing in this appendix result from the computer listing of the raw data collected from the tests after it has been key punched onto data processing cards. The data required the use of 62 columns of the general purpose 80 column card with the following information provided in each column:

Column	Information
1	The Figure 1 indicates data from the factorial designed tests and A, B, C, D indicates data from acceptance tests 1, 2, 3 and 4 respectively. Letters M through T indicate data from Special Tests 1 through 8 respectively.
2	Blank.
3,4,5,6	Range. (Ft.)
7	Blank.
8,9,10	Miss Distance. (Ft.)
11	Blank.
12,13,14,15	Aircraft Altitude. (Ft.)
16	Blank.
17,18	Aircraft Speed. (Knots)
19	Blank.
20,21,22	Aircraft heading of 0, 90, 180, 270 indicate the firing position was located to the left of, aft of, to the right of, and in front of the aircraft at time of test.
23,24	Blank.
25, 26, 27	Type of weapon fired.

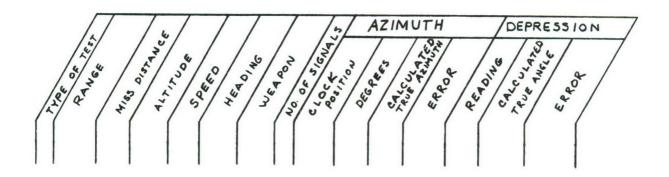
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Column	Information
28	Blank.
29	Number of signals reported as appearing on the scope.
30	Blank.
31,32,33,34	The reported clock reading regarding azimuth location of gun position.
35	Blank.
36,37,38	The reported clock position converted to degrees. (1200 being 0° degrees or 360°.)
39	Blank.
40, 41, 42	The calculated azimuth in degrees for the indicated test condition.
43	Blank.
44,45,46,47	The variation in degrees from the reported azimuth and the calculated azimuth. Negative values indicate reading was in clockwise direction from calculated reading except on acceptance test data. Negative values of acceptance test data indicate error in counterclockwise direction.
48,49	Blank.
50,51	Depression angle reading. (Degrees)
52	Blank.
53,54,55,56	Calculated depression angle. (Degrees)
57	Blank.
58,59,60,61,62	Variation in degrees from reading and calculated angle. Negative values indicate excessive reading angle.

1 1200 300 200 20 0 M14 1 300 090 284 -166 15 9.2 5.8

FIGURE A-1: EXAMPLE OF CARD HEADING

(U)As an aid in reading the computer listing of raw data, figure A-2 is provided which reveals a column heading for each of the columns in the listing. This temperature type figure could be cut out and placed over the columns on each page to facilitate reading initially.



(U) FIGURE A-2. COLUMN HEADINGS

(\$) FACTORIAL TEST DATA

SUNFICENTIAL

1	500	300	50	20	90	M16	0			21	1		4.9	
1	500			20		M16	0			12			4.9	
1	500			20		M16		115	037	03	1 -6	30		
1	500			20		M16				30	1	30	4.9	25.1
1	500			20		M14	1						4.9	
1	500		-	20		M14							4.9	
1	500 500			20		M14			037			30		
1	500			20		M14						30		
1	500		200	20		500	2					45		
1	500		-	20		50C	3					45		
1	500			20		50C	2					30		
1	500			40		M16	1		247			30 45		
1	500		50	40		M16	2		135			30		
1	500		50	40		M16	2					30		
1	500	300	50	40		M16	2		300			30		
1	500	300	50	40	90	M14	3	720				30		
1	500		50	40	180	M14	2	430	135	121		30		
1	500	300	50	40	270	M14	2	100	030	031	1	35	4.9	30.1
1	500	300	50	40	0	M14	3	1000	300	301	1	30	4.9	25.1
1	500	300	50	40	90	50C	2	715	217	211	-6	35	4.9	
1	500		50	40	180	50C	2	415	127	121		35	4.9	30.1
1	500	300	50	40		50C	2	115	037			30	4.9	25.1
1	500	300	50	40	0	50C	1	1130	345			40	4.9	35.1
1	500	300	50	80	90	M16	1	815	247			40	4.9	35.1
1	500	300 300	50	80	180	M16	3	415	127	121		30	4.9	
1	500	300	50 50	80	270	M16	1	100	030	031		40	4.9	35.1
1	500	300	50	83	90	M16 M14	3	700	300 210			30	4.9	25.1
1	500	300	50	80	180	M14	3	415	127	211		30	4.9	25.1
1	500	300	50	80	270	M14	2	115	037	031		30	4.9	25.1
1	500	300	50	80	0	M14	2	1000	300	301		30	4.9	25·1 25·1
1	500	300	50	80	90	50C	1	800	240	211		30	4.9	25.1
1	500	300	50	80	180	50C	2	400	120	121		30	4.9	25.1
1	500	300	50	80	270	50C	1	210	065	031		30	4.9	25.1
1	500	300	50	80	0	50C	2	1000	300	301		30	4.9	25.1
		202												
1	500	300	200	20	90	M16	2	715	217	211		30	19.0	11.0
1	500	300	200	20	180	M16	2	430	135	121		40	19.0	21.0
1	500	300	200	20	270	M16	3	100	030	031		45	19.0	26.
1	500	300	200	20	90	M16 M14	2	1015	307	301		30	19.0	11.
1	500	300	200	20	180	M14	2	430	217		-6 -14		19.0	
1	500	300	200	20	270	M14	2		030	121	1	30	19.0	11.
1	500	300	200	20	0		2	1000	300	301	1	35	19.0	21.
1	500	300	200	20	90	50C	3		217	211	-6	45		26.
1	500	300	200	20	180	50C	2	430	130	121	-9	40	19.0	
1	500	300	200	20	270	50C	2	115		031	-6	35	19.0	16.
1	500	300	200	20	O	50C	1	1100	330	301	-29	45	19.0	26.
1	500	300	200	40	90	M16	2	700	210	211	1	45	19.0	
1	500	300	200	40	180	M16	2	415	127	121	-6	40	19.0	21.
1	500	300	200	40	270		3		030		1	40	19.0	
1	500	300	200	40	0	M16		1000		301	1	35	19.0	16.
1	500	300	200	40	90		3		217		-6	35	19.0	16.
1	500	300	200	40	180		3			121	1	40	19.0	21.
1	500	300	200	40	0	M14	2		037		-6	40	19.0	21.0
1	500	300	200	40	90		2		300 217	301	1	35	19.0	
1			200		180		2			121	-6 -6	30 35	19.0	11.
1	500		200		270		2		040		7		19.0	
						THE		DENT	117				H. Incin.	1
					6.00	-Co op 14	ğ x	F4 14 1	F Se N		- 4.4			

CONSULARIANT TURICLASSIFIED

										-	- March Strike - or School on Annual Property and the Control of t			
1	500	300	200	40	0	50C	1	1100	330	301	1	45	19.0	26.
1	500	300	200	80	90	M16	3		210	211	1	30	19.0	
1	500	300	200	80	180	M16	2	415	127	121	-6	30	19.0	11.
1	500	300	200	80	270	M16	3	100	030	031	1	45	19.0	
1	500	300	200	80	0	M16	2	1000	300	301	î	40	19.0	21.
1	500	300	200	80	90	M14	2	700	210	211	î	30	19.0	11.
1	500	300	200	80	180	M14	2	430	135	121	-14	30	19.0	11.0
1	500	300	200	80	270	M14	2	110	035	031	-4	45	19.0	26.
1	500	300	200	80	0	M14	2	945	292	301	8	40	19.0	21.0
1	500	300	200	80	90	50C	2	645	202	211	8	20	19.0	1.0
1	500	300	200	80	180	50C	2	420	130	121	-9	30	19.0	11.0
1	500	300	200	80	270	50C	2		030		1	45	19.0	
1	500	300	200	80	0	50C	2	945	292	301	8	60	19.0	
•	, , ,	300	200	00	0	300	-	777	272	301	0	00	19.0	41.0
1	500	300	500	20	90	M16	2	715	217	211	-6	45	40.6	4.4
1	500	300	500	20	180	M16	2	445	144	121	-23	70	40.6	
1	500	300	500	20	270	M16	1	100	030	031	. 1	70	40.6	
1	500	300	500	20	0	M16	3	1000	300	301	1	45	40.6	4.4
1	500	300	500	20	90	M14	2	715	217	211	-6	45	40.6	4.4
1	500	300	500	20	180	M14	2	445	142	121	-21	45	40.6	4.4
1	500	300	500	20	276	M14	2	115	037	031	-6	50	40.6	9.4
1	500	300	500	20	0	M14	2	950	295	301	6	45		4.4
1	500	300	500	20	90	50C	2	715	217	211	-6	45	40.6	4.4
1	500	300	500	20	180	50C	4	500	150	121	-29	45	40.6	4.4
1	500	30C	500	20	270	50C	4	115	037	031	-6	60		19.4
1	500	300	500	20	0	50C	3	1000	300	301	1	45	40.6	4.4
1	500	300	500	40	90	M16	2		210	211	1	40	40.6	
1	500	300	500	40	180	M16	2	500	150	121	-29	45		4.4
1	500	300	500	40	270	M16	2		037	031	-6		40.6	
1	500	300	500	40	0	M16	2	935	287	301	3		40.6	9.4
1	500	300	500	40	90	M14	2	715	217	211	-6	30		-10.6
1	500	300	500	40	180	M14	2	445	142	121	-21		40.6	4.4
1	500	300	500	40	270	M14	3	100	030	031	1	60	40.6	19.4
1	500	300	500	40	0	M14	3	1000	300	301	1		40.6	4.4
1	500	300	500	40	90	50C	3	715	217	211	-6	40	40.6	-0.6
1	500	300	500	40	180	50C	3	445	142	121	-21	50	40.6	9.4
1	500	300	500	40	270	50C	3	115	037	031	-6	55	40.6	14.4
1	500	300	500	40	0	50C	3	1000	300	301	1	45	40.6	4.4
1	500	300	500	80	90	M16	2	715	217	211	-6	30	40.6	-10.6
1	500	300	500	80	180	M16	3	445	142	121	-21	45	40.6	4.4
1	500	300	500	80	270	M16	3	100	030	031	1	50	40.6	9.4
1	500	300	500	80	0	M16	2	945	292	301	8	45	40.6	4.4
1		300		80	90	M14			210		1		40.6	-5.6
1		300		80	180	M14			135	121	-14		40.6	4.4
1	500	300	500	80	270	M14	2	100	030	031	1		40.6	19.4
1		300		80	0	M14	2		292		8	50	40.6	9.4
1			500	80	90	50C	2		210		1		40.6	4.4
1		300		80	180	50C	1	500		121	-29		40.6	4.4
1		300		80	270	50C	3	100	030		1		40.6	19.4
1	500	300	500	80	0	50C	2		285		6		40.6	4.4

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1	750	200	200	40	270			1235	015	015		30	14.5	15.5
1	750		200		180	50C		400	120	105	1.5	. 30	14.5	15.5
1		200	200	40	90	50C	2		210		-15		14.5	15.5
1		200	200	40	0		2		195		90		14.5	45.5
1		200	200		270	M14		1230			0		14.5	15.5
1	750	200	200		180	M14				105	more. In		14.5	•
1	750	200	200	40	90		2	700	210		-15	30	14.5	15.5
1	750		200	40	0		2		285		0	30	14.5	15.5
1		200			270		1		075		-60	30	14.5	15.5
1	750	200	200		180		2			105	-15	30	14.5	15.5
1		200	200	40	90	M16	1		255		-60	35	14.5	20.5
1	750	200	200	20	0		3		285		0	30	14.5	15.5
1	750	200	200	20	270	50C			015		0	30	14.5	15.5
1	750	200	200	20	180		1			105	-60	35	14.5	20.5
1		200	200	20	90	50C			210		-15	30	14.5	15.5
1		200	200	20	0	M14			285		0	30	14.5	15.5
1		200		20	270	M14		1215			-7	30	14.5	15.5
1		200			180	M14	3		090		15	35	14.5	20.5
						M14			240		-45	30	14.5	15.5
1			200	20	0	M16	1	920						15.5
1				20				430	135	015	-120	30	14.5	15.5
	750				180		1	400	120	105	-15	35	14.5	20.5
					90	M16	1	645	202	195	-7	30	14.5	15.5
1	750	200	200	2.0	00	142			2	1				
1	750	200	50	80	0	50C	2	915	277	285	7	30	3.7	26.3
1	750			80	270	50C	2	1230	015	015	0	30		26.3
1	750		50		180		2	400	120	105	-15	30	3.7	
1	750		50	80				815				35		31.3
1	750		50		0			530				30	3.7	26.3
1	750		50		270			1230					3.7	
1			50		180	M14	2	400	120	105	-15		3.7	
1	750		50		90			815						31.3
	750				0	M16	3	900	2/7	285	15	30		26.3
1	750		50		270	M16	3	1230	015	015	0	30		
1	750		50		180	MIC	0	1220	015	105	0 15	20		
1	750		50				0	645	202	195	- /	30		
1	750		50		90						-45 -7		3 0 7	46.3
1	750		50		0						-45			
1	750		50		270						-19			
1	750		50		180	500	2	400	120	105	-15	30	3.7	
1	750				90			830						
1	750		50		0	M14	2	930	285	285	0	30		
1	750		50		270	M14	3	1230	015	015	0	30		26.3
1	750		50		180								3.7	
1	750				90						-45			
1	750		50		0						0			21.3
1	750		50		270	M16	7	1230	015	015	0	30		26.3
1	750		50		180						-15			
1	750		50		90						-60			
1	750		50	20		50C	1	1100	330	285	-45			
1	750		50		270	50C	1	400	120	015	-105	30	3.7	26.3
1	750		50		180	50C	0			105			3.7	
1		200	50	20	90						-60			
1		200	50	20							-45			26.3
1	750		50	20	270	M14	3	1230	015	015	0	30	3.7	26.3
1		200	50	20	180	M14	0			105			3.7	•
1		200	50	20		M14	0			195			3.7	•
1		200	50	20	0	M16	1	1100	330	285	-45	30	3.7	26.3
1	750		50		270	M16	2	1230	015	015		0 30	3.7	26.3
1	750	200	50	20	180	M16	0			105	_		3.	
1	750		50	20	90	M16	1	815	247	195	-52	35	3.7	31.3
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															and the a	
		1	750	200	200	40	0	50C	2	030	285	285	0	30	14.5	15.5
		_								36, 963,946						
		1		200		80	90	M16			255		-60		14.5	25.5
		1	750	200	200	80	180	M16			120		-15	30	14.5	15.5
		1	750	200	200	80	270	M16	1	1230	015	015	0	40	14.5	25.5
		1	750	200	200	80	0	M16			270		15			15.5 AB
		1		200									-120			
							270	M16							14.5	15.5
		1		200		80	90	M14			195		0		14.5	15.5
		1	750	200	200	80	180	M14	2	400	120	105	-15	30	14.5	15.5
		1	750	200	200	80	0	M14	2	915	277	285	7	30	14.5	15.5
		ī		200		80	90	50C			195		ó		14.5	15.5
		1			200		180	50C			120		-15		14.5	15.5
		1	750	200	200	80	270	50C	2	430	135	015	-120	30	14.5	15.5
		1	750	200	200	80	0	50C	2	915	277	285	7	30	14.5	15.5
		1	750	200	500	20	90	M16	2	700	210	105	-15	40	33.0	7.
		1	75 0			20	180	M16			120		-15		33.0	2.
		1	750	200	500	20	270	M16	2	1200	000	015	15	60	33.0	27.
		1	750	200	500	20	0	M16	2	920	280	285	5	35	33.0	2.
		1	750	200	500	20	90	M14			210		-15	40	33.0	7.
				200							120				33.0	
		1				20	180	M14					-15			12.
		1		200		20	270	M14		1230			0		33.0	12.
		1	750	200	500	20	0	M14	1	630	195	285	90		33.0	27.
		1	750	200	500	20	90	50C	1	700	210	195	-15	60	33.0	27.
		1	750	200	500	20	180	50C	2	400	120	105	-15		33.0	12.
		1	750	200		20	270	50C			075		-60		33.0	32.
					-											
		1		200		20	0	50C			270		15		33.0	12.
		1		200		40	90	M16	1	830	255	195	-60	45	33.0	12.
		1	750	200	500	40	180	M16	2	430	135	105	-30	40	33.0	7.
		1	750	200	500	40	270	M16	1	230	075	015	-60	35	33.0	2.
		1		200		40	0	M16			270		15		33.0	7.
		1		200		40	90	M14			195		O		33.0	-3.
,		1	750	200			180	M14			127		-22		33.0	2.
		1		200		40	270	M14	2	100	030	015	-15	35	33.0	2.
		1	750	200	500	40	0	M14	2	530	165	285	120	35	33.0	2.
		1	750	200	500	40	90	50C	2	700	210	195	-15	35	33.0	2.
		1		200	500	40	180	50C			135		-30		33.0	2.
		î		200				50C					-160			
						40	270								33.0	17.
		1		200	500	40	0	50C			270		15		33.0	12.
		1	750			80	90	M16	2		200		-5		33.0	-3.
		1	750	200	500	80	180	M16	3	400	120	105	-15	45	33.0	12.
		1	750	200	500	80	270	M16	2	1250	025	015	-10	50	33.0	17.
		1		200		80	0	M16			150		135		33.0	12.
		î			500		90			640						
													-5		33.0	-3.
		1		200			180			415			-22		33.0	7.
		1		200		80	270			1250			-10	50	33.0	17.
		1	750	200	500	80	0	M14	2	900	270	285	15	55	33.0	22.
		1			500	80				650					33.0	-3.
		1					180			515					33.0	12.
	3				500											
		1								1250					33.0	17.
		1	150	200	500	80	0	50C	2	500	150	285	135	45	33.0	12.
		1	750	300	50	20	90	M16	1			202			3.5	•
		1	750		50		180								3.5	
	2	î	750		50		270	M16	2	1216	007	022	14	20		26.5
								1410	2	1219	201	222	14	30	3.5	26.5
7.		1	150	300	.50		0						-38			
			750		50		90	M14		815	247	202	-45	35		31.5
		1		300	50	20	180	M14				Programme and American	WWTHIS Fin hold In		3.5	•
		1	750	300	50		270			1200	000	022	22	50	3.5	46.5
					-	_ •		-	1	PIDE	-	-B.	55	al Vi	1. L. J. 15.	A-9
									11/	FIRE	TH	FT -	sound that My had I have belonged		-	H-7
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	750						1000							
1	750		50	20	0	M14	2	930	285	292	7	20	3.5	16.5
1	750	300	50	20	90	50C							3.5	•
1	750	300	50	20	180	50C	1	515	157	112	-45	30	3.5	26.5
1	750	300	50	20	270	50C	1	1245		022	0	30	3.5	26.5
1	750	300	50	20	0	50C	i	930	285		7	30	3.5	
														26.5
1	750	300	50	40	90	M16	1	830	255	202	-53	30	3.5	26.5
1	750	300	50	40	180	M16	0						3.5	•
1	750	300	50	40	270	M16	1	1250	025	022	-3	30	3.5	26.5
1	750	300	50	40	0	M16	2		210		82	45	3.5	41.5
1	750	300	50	40	90	M14		,00	210	212	02	42		
			12					100	100	110		-	3.5	•
1	750	300	50	40	180	M14	2		120		-8	30	3.5	26.5
1	750	300	50	40	270	M14	2	100	030	022	-8	30	3.5	26.5
1	750	300	50	40	0	M14	1	930	285	292	7	30	3.5	26.5
1	750	300	50	40	90	50C	1	830	255	202	-53	35	3.5	31.5
1	750	300	50	40	180	50C	0						3.5	•
1	750	300	50	40	270	50C	1	100	030	022	-8	35	3.5	31.5
1	750	300												
			50	40	0	50C	2	930	285	292	7	30	3.5	26.5
1	750	300	50	80	90	M16							3.5	
1	750	300	50	80	180	M16	1	400	120	112	-8	30	3.5	26.5
1	750	300	50	80	270	M16	2	1250	025	022	-3	40	3.5	36.5
1	750	300	50	80	0	M16	2	1220	010	292	-78	30	3.5	26.5
1	750	300	50	80	90	M14	2		240		-38	40	3.5	
	750							800	240	202	-30	40		36.5
1		300	50	80	180	M14	0						3.5	
1	750	300	50	80	270	M14	3	1230			7	35	3.5	31.5
1	750	300	50	80	0	M14	3	930	285	292	7	30	3.5	26.5
1	750	300	50	80	90	50C	2	600	180	202	22	60	3.5	56.5
1	750	300	50	80	180	50C	2	100	030	112	92	35	3.5	31.5
1	750	300	50	80	270	50C	2	950	295	022	87	30	3.5	26.5
1	750	300	50	80	0	50C			285					
1	100	500	50	00	U	200	2	930	200	292	7	30	3.5	26.5
	750	000					-							
1	750	300	200	20	90	M16	1		255		-53	45	13.9	31.1
1	750	300	200	20	180	M16	2	400	120	112	-8	45	13.9	31.1
1	750	300	200	20	270	M16	2	100	030	022	-8	45	13.9	31.1
1	750	300	200	20	0	M16	2	945	292	292	0	30	13.9	16.1
1	750	300	200	20	90	M14	1		255		-53	40	13.9	26.1
1	750	300	200	20	180	M14	2	345	112	112				
1	750	300									0	30	13.9	16.1
			200	20	270	M14	3	1245	022		0	30	13.9	16.1
1	750	300	200	20	0	M14	2	930		292	7	30	13.9	16.1
1	750	300	200	20	90	50C	2	645	202	202	C	30	13.9	16.1
1	750	300	200	20	180	50C	2	400	120	112	-8	45	13.9	31.1
1	750	300	200		270	50C		1245	022	1101	0	35	13.9	21.1
1	750	300	200	20	0	50C			285		7		13.9	
1	750	300		40								_		16.1
					90	M16			202		0		13.9	16.1
1	750	300	200	40	180	M16	2	500		112	38	40	13.9	26.1
1	750	300	200	40	270	M16	2	100	030	022	8	40	13.9	26.1
1	750	300	200	40	0	M16	2	945	292	292	0	30	13.9	16.1
1	750	300	200	40	90	M14	2	645	202	202	0	30	13.9	16.1
1	75C	300	200	40	180	M14	1	515	157	112	45	30	13.9	16.1
1	750	300	200	40	270	M14	2	100	030	022				
1	750	300									-8	35	13.9	21.1
			200	40	0	M14	2	530		292	127	30	13.9	16.1
1	750	300	200	40	90	50C		645		202	0	30	13.9	16.1
1	750	300	200	40	180		2	500	150	112	-38	30	13.9	16.1
1	750	300	200	40	270	50C	2	100	030	022	-8	40	13.9	16.1
1	750	300	200	40	0	50C		530		292	127	30	13.9	16.1
											'	- 0		1
1	750	300	200	40	90	M16	3	700	210	202	-0	20	12 0	16 1
1	750	300	200		180						-8	30	13.9	16.1
							3			112	-8	35	13.9	21.1
1	750	300	200	40	270		3		030		-8	35	13.9	21.1
1	750	300	200	40	0	M16			290		2	30	13.9	16.1
1	750	300	200	40	90	M14	4	700	210	202	-8	35	13.9	21.1
						4	71	HIM	AT	基準	(. (<u>. (.)</u>			A-10

CONCINENTIAL A-10



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								•						
1	750	300	200	40	180	M14	2	400	120	112	-8	35	13.9	21.1
1	750	300	200	40	270	M14	3		030		-8	35	13.9	21.1
1	750	300	200	40	0	M14	3	950	295	292	-3	30	13.9	16.1
1	750	300	200	40	90	50C	2	635	197	202	4	30	13.9	16.1
1	750	300	200	40	180	50C	2	400	120	112	-8	40	13.9	26.1
1	750	300	200	40	270	50C	2	100	030	022	-8	35	13.9	21.1
1	750	300	200	40	0	50C	2	350	115	292	177	30	13.9	16.1
1	750	300	500	20	90	M16	2	700	210	202	-8	30	31.8	-1.8
1	750	300	500	20	180	M16	2	430	135	112	-23	40	31.8	8.2
1	750	300	500	20	270	M16	3	100	030	022	-8	40	31.8	8.2
1	750	300	500	20	0	M16	2	930	285	292	7	35	31.8	3.2
1	750	300	500	20	90	M14	2	700	210	202	-8	35	31.8	3.2
1	750	300	500	20	180	M14	2	400	120	112	-8	40	31.8	8.2
1	750	300	500	20	270	M14	3	1230	015	022	7	40	31.8	8.2
1	750	300	500	20	0	M14	4	900	270	292	22	40	31.8	8.2
1	750	300	500	20	90	50C	3	700	210	202	-8	35	31.8	3.2
1	750	300	500	20	180	50C	2	400	120	112	-8	40	31.8	8.2
1	750	300	500	20	270	50C	4	1230	015	022	7	40	31.8	8.2
1	750	300	500	20	0	50C	3	900	270	292	22	35	31.8	3.2
1	750	300	500	40	90	M16	2	700	210		-8	30	31.8	-1.8
1		300	500	40	180	M16	2	430	135	112	-23	35	31.8	3.2
1	750	300	500	40	270	M16	3	1200	000	022	22	10	31.8	-21.8
1	750	300	500	40	0	M16	2	920	280	292	12	40	31.8	8.2
1	750	300	500	40	90	M14	3	700	210		-8	30	31.8	-1.8
1	750	300	500	40	180	M14	2	400		112	-8	40	31.8	8.2
1	750	300	500	40	270	M14	2	1240	020		-8	45	31.8	13.2
1	750	300	500	40	0		3		280		12		31.8	13.2
1	750	300	500	40	90	50C	3		210		-8	35	31.8	3.2
1	750	300	500	40	180	50C	2	430	135		-23		31.8	13.2
1	750	300	500	40	270	50C	3		025		-3		31.8	13.2
1	750	300	500	40	0	50C		930	285		7		31.8	8.2
1	750	300	500	80	90	M16	-	800	240		-38		31.8	8.2
1	750	300	500	80	180	M16	2	400	120		-8		31.8	8.2
1	750	300	500		270	M16			010		12		31.8	3.2
1	750	300	500	80	0	M16	1	1030	315		-23		31.8	38.2
1	750	300	500	80	90	M14	1	800		202	-38	40	31.8	8 • 2
1	750	300	500	80	180	M14	3	345		112	0	25	31.8	-6.8
1		300	500	80	270			1240	020		2		31.8	8 • 2
1	750	300	500	80	O	M14	1	1100	330		-38		31.8	28.2
1	750	300	500	80	90		2	650	205		-3	30	31.8	-1.8
1	750	300	500	80	180	50C	1	500	150	112	-38	45	31.8	13.2
1	750	300	500	80	270		2	100	030		-8		31.8	13.2
1	750	300	500	80	0	50C	3	500	150	292	142	30	31.8	-1.8

TECHNICAL LIBPARY
BLDG. 305
ABERDEEN PROVING GROUND, MD.,
STEAP-TL



CHI	HTW	社社	
CEAH!	HILL	THE	

	BRELASSIFIED													
						Carrie .	•••				UNGLA	334		
1	1000		50	20	90	M16				191			2.8	•
1	1000		50	20	180 270	M16		1215	007	101	3	20	2.8	27 2
1	1000		50	20	0			1215			-45	30	2.8	27.2
1	1000		50	20	90			800				35	2.8	32.2
1	1000		50	20	180						-4	35	2.8	32.2
1	1000		50		270			1200				30	2.8	27.2
1	1000		50 50	20	90	M14		1050	325			35 35	2.8	32·2 32·2
1	1000		50		180	50C		500			-49	30	2.8	27.2
1	1000		50		270	50C		200			-49	30	2.8	27.2
1	1000		50	20	0	50C	2	100	030	281	-109	45	2.8	42.2
1	1000		50	40	90			730			-34	40	2.8	37.2
1	1000		5 0		180 270			500 1215			-49 3	30	2.8	27.2
1	1000		50	40	0			1045				30 35	2.8	27·2 32·2
1	1000		50	40	90			745				35	2.8	32.2
1	1000		50		180			320			1 3	30	2.8	27.2
1	1000		50		270			1215				30	2.8	27.2
1	1000		50	40	90			1100 800			-49 -49	30 30	2.8	27·2 27·2
1	1000		50		180			520			-59	30	2.8	27.2
1	1000	200	50		270	50C	2	1215	007	011	3	60	2.8	57.2
1	1000		50	40	0			1100				40	2.8	37.2
1	1000		5 0	80	90 180			700 420			-19 -29	40	2 • 8	37.2
1	1000		50		270			1220			1	15	2.8	12·2 57·2
1	1000		50	80	0			1045			-41	45	2.8	42.2
1	1000		50	80	90	M14		800			-49	30	2.8	27.2
1	1000		50		180			330			-4	30	2.8	27.2
1	1000		50 50	80	270			1215 1050			-44	35 30	2.8	32·2 27·2
1	1000		50	80	90			750				30	2.8	27.2
1	1000		50	80	180			330			-4	30	2.8	27.2
1	1000		50		270			1215			3		2.8	32.2
1	1000	200	50	80	0	300	2	300	090	281	-169	30	2.8	27.2
1	1000			20	90			800	240	191	-49	30	11.1	18.9
_	1000				180	M16			150				11.1	
1	1000		200	20	270	M16		1230			-4 -19		11.1	18.9
1	1000		200	20	90	M14		815	247	281 191	-56		11.1	33.9
1	1000		200	20	180	M14		500	150	101	-49		11.1	18.9
1	1000		200	20	270	M14		1230		011	-4		11.1	23.9
1	1000	200	200	20	0	M14			277	281	3		11.1	18.9
1	1000		200	20	90 180	50C		345	202	191	-11 -11		11.1	23.9
1		200	200	20	270	50C		1230	015	011	-4		11.1	23.9
1	1000	200	200	20	0	50C		915	285	281	-4	25	11.1	13.9
1	1000		200	40	90	M16		720		191	-29		11.1	28.9
1	1000		200	40	180 270	M16		1245	115	011	-14 -11		11.1	28.9
1	1000		200	40	0	M16			100	281	-179		11.1	23.9
1	1000	200	200	40	90	M14	1		247	191	-56	35	11.1	23.9
1	1000		200	40	180	M14			115	101	-14	35	11.1	23.9
1	1000	200	200	40	270	M14		1245		011	-11		11.1	23.9
1		200	200	40	90	50C			285	281	-4 -11		11.1	18.9 18.9
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						West St.								

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1 1 1	1000 1000 1000	300	50 50 50		180 270 0	M14 M14 M14	1	200	060	107	-43	15	2.7	12.3
1	1000	300 300	50 50	20	90	M16 M14	1	1100 800		287 197	-43 -43	0 30	2.7	-2.7 27.3
1 1 1	1000 1000 1000	300	50 50		90 180 270	M16 M16 M16	1		240 105		-43 2	30 45	2.7 2.7 2.7	27·3 42·3
1			200	00	Ü	500	-	500	0,0	201	107	00	2011	3.7
1	1000	200	500		270		2	1220	010	011	1-169	50	26.1	23.9
1	1000			80	90 180	50C			192 120		-1 -19	30	26.1 26.1	3.9
1	1000			80	270	M14 M14		1230 900	270	011	-4 11		26.1 26.1	18.9
1	1000				180	M14			115		-14		26.1	3.9
1	1000	200	500	80	90	M14	2	630	195	191	-4		26.1	3.9
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1	1000	200	50 0	80	180 270	M16	1	400 1220	120 010	101	-19	35	26.1	8.9
1	1000	200	500	80	90	M16		630	195	191	-4	30	26.1	3.9
1	1000	200	500	40	0		3	920	280	281	1	30	26.1	3.9
1	1000		500	40	180	50C	5	400 1230	120	101	-19 -4	40	26.1	13.9 18.9
1	1000	200	500	40	90		4	630	195	191	-4		26.1	3.9
1	1000		500	40	0	M14	3	920	280	281	1		26.1	18.9
1	1000	200	500	40	270	M14		1210	120	101	-19 6	50	26.1	18.9
1	1000		500	40	90	M14 M14	3	400	205	191	-14	45	26.1	18.9
1	1000		500	40	0	M16	1	1100	330	281	-49	50	26.1	23.9
1	1000		500	40	270	M16		1215	007	011	3	45	26.1	18.9
1	1000		500	40	180	M16		400	195	191	-4 -19		26.1	3.9
1	1000	200	500	20	90	50C M16		900	270	281	11	30	26.1	3.9
1	1000	1	500	20	270	50C		1230		011	-4	45	26.1	18.9
1	1000	200	500	20	180	50C		400	120	101	-19		26.1	13.9
1	1000	200	500	20	90	50C	2	630	195	191	-109			33.9 8.9
1	1000	200	500	20	270	M14	1	200 300	060	011 281	-49 -169	30	26.1	3.9
1	1000		500	20	180	M14		330	105	101	-4		26.1	13.9
1	1000		500	20	90	M14		640		191	-9	30	26.1	3.9
1	1000		500	20	0	M16		910	275	281	6	30	26.1	3.9
1	1000	200	500 500	20	180 270	M16	2	345 200	112	101	-11 -49		26.1	18.9
1	1000	200	500	20	90	M16			240	191	-49		26.1	13.9
1	1000	200	200	80	0	50C	2	900	270	281	11	30	11.1	18.9
1	1000				270	50C		1215			3		11.1	-1 • 1
1		200	200		180	50C	2	330	105	101	-4		11.1	18.9
1	1000	200	200	80	90	50C		800	240	191	-49		11.1	28.9
1	1000	200	200	80	270	M14		1230	015	011 281	-4 -109	30 45	11.1	18.9
1	1000	200	200	80	180	M14	1	430	135	101	-34	10	11.1	-1 • 1
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i	1000		200	80	0	M16		1100		281	-49	45	11.1	33.9
1	1000	200	200	80	180 270	M16	0	1230	015	011	-4	40	11.1	28.9
1	1000	200	200	80	90	M16		800	240	191	-49	30	11.1	18.9
1	1000	200	200	40	0	50C	2	920	280	281	1	20	11.1	8.9

CHOLASSEASE |

1	1000		50	20	90	50	1	800	240	197	-43	30	2.7	27.3	
1	1000	300	50	20	180	50							2.7		
1	1000	300	50	20	270	50	20-23		060		-43	0	2.7		
1		300	50	20	0	50		1100	330	287	-43	15	2.7		
1	1000	300	50	40	90	M16							2.7		
1	1000	300	50	40	180	M16		500		107	-43	25	2.7	111111111111111111111111111111111111111	
1	1000		50 50	40	270	M16		100 1100		017 287	-13 -43	30	2.7		
1	1000	300	50	40	90	M14			240	197	-43	15	2.7	12·3 27·3	
1	1000		50	40	180	M14		500		107	-43	20	2.7	1.7.3	
1	1000		50		270	M14		100		017	-13	30	2.7	27.3	
1	1000		50	40	0	M14			180		107	40	2.7	37.3	
1	1000	300	50	40	90	50	1					30	2.7	27.3	
1		300	50	40	180	50	1	500	150	107	-43	20	2.7	17.3	
1	1000	300	50		270	50		1230	015	017	2	30	2.7	27.3	
1	1000		50	40	0	50		1100	330	287	-43	30	2.7	27.3	
1	1000		50	80	90	M16							2.7	•	
1	1000	300	50	80	180	M16			150		-43	15	2.7	12.3	
1	1000	300	50	80	270	M16		1230			-43	30	2.7	27.3	
1	1000		50	80	90	M16		1100	240		-43	30 25	2.7	27.3	
1	1000		50		180	M14		800	240	191	-43	25	2.7	22.3	
1	1000		50	80	270	M14		100	030	017	-13	45	2.7	42.3	
1	1000		50	80	0	M14		1100		287	-43	30	2.7	27.3	
1	1000		5 C	80	90	50		800		197	-43	25	2.7	22.3	
1	1000	300	50	80	180	50	2	400		107	-13	30	2.7	27.3	
1	1000		50		270	50			060		-43	20	2.7	17.3	
1	1000	300	50	80	0	50	1	1100	330	287	-43	30	2.7	27.3	
1	1000	300	200	20	90	M16	1	800	240	197	-43	30	10.9	19.1	
1		300	200		180	M16		500	150	107	-43	35			
1	1000	300	200		270	M16		200		017	-43	45		34.1	
1	1000	300	200	20	0	M16		930		287	2	0		-10.9	
1	1000		200	20	90	M14	1	830	255	197	-58	30		19.1	
1		300	200		180	M14				107			•	•	
1	1000		200		270	M14		1230			2		10.9		
1	1000		200	20	0	M14		830	255		32			-10.9	
1	1000		200	20	90	50		830		197	-58		10.9		
1		300	200	20	180 270	50	3	400	120	107	-13		10.9	19.1	
1	1000			20	0	50		930	075 285	017	-5 8		10.9	19.1	
1		300		40	90	M16		820						19.1	
1	1000				180	M16			120		-13		10.9	19.1	
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1	1000	300	200	40	0	M16		930	285	287	2	0	10.9	-10.9	
1	1000	300	200	40	90	M14	1000	810	245	197	-48	25	10.9	22.3	
1		300	200	40	180	M14		520	160	107	-53	30	10.9	19.1	
1	1000	300	200	40	270	M14		210	065	017	-48	25	10.9	14.1	
1	1000	300 300	200	40	0	M14	3	930		287	2	15	10.9	4.1	
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1	1000	300	200	40	0	50	3	920	280	287	-3 7	30	10.9	19.1	
ì	1000	300	200	80	90	M16		810	245	197	-48	25	10.9	14.1	
1		300	200	80	180	M16		340	110	107	-3	25	10.9	14.1	
1	1000		200	80	270	M16		1230		017	2		10.9	19.1	
1	1000	300	200	80	0	M16				287	42	0	10.9	-10.9	
1		300	200	80	90	M14		700		197	-13		10.9	54.1	
1	1000		200		180	M14		400		107	-13		10.9	19.1	
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	1000	300	200	80	0	M14	3	830	255	287	32	0	10.9	-10.9
1	1000	300	200	80	90	50	2	830	255	197	-58	25	10.9	14.1
1	1000	300	200	80	180	50	1	520	160	107	-53	25	10.9	
1	1000	300	200	80	270	50	2	1240	020	017	-3	40	10.9	
1	1000	300	200	80	0	50				287	37	50	10.9	
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1	1000	300	500	20	90	M16	1	820	250	197	-53	30	25.6	4.4
1	1000	300	500	20	180	M16	1	410	125		-18		25.6	9.4
1	1000	300	500	20	270	M16	2	1240	20		-3		25.6	19.4
1	1000	300	500	20	0	M16	1	1100	330		-43	45	25.6	19.4
1	1000	300	500	20	90	M14	2	700	210		-13	30	25.6	4.4
1	1000	_	500	20	180	M14	2	430	135	107	-28	35		9.4
1	1000	300	500	20	270	M14	3	100	30	017	-13		25.6	19.4
1	1000	300	500	20	0	M14	3	820	250		37		25.6	4.4
1	1000	300	500	20	90	50	3	700	210	197	-13	30	25.6	4.4
1	1000	300	500	20	180	50	3	410	155	107	-48	35		9.4
1	1000	300	500	20	270	50	3	1240	20	017	-3	40	25.6	14.4
1	1000	300	500	20	0	50	4	930	285		2	25	25.6	6
1	1000		500	40	90	M16	2	700		197	-17	30	25.6	4.4
1	1000	300	500	40	180	M16	2	400	120		-13	30	25.6	4.4
1	1000	300	500	40	270	M16	3	1240	20	017	-3	45	25.6	19.4
1		300	500	40	0	M16	2	930	285	287	2	25	25.6	6
1		300	500	40	90	M14	3	650	205	197	-8	30	25.6	4.4
1	1000		500	40	180	M14	3	420	130	107	-23	35	25.6	9.4
1		300	500	40	270	M14	2	1240	20	017	-3	45	25.6	19.4
1		300	500	40	0	M14	2	1100	330	287	-43	75	25.6	49.6
1		300	500	40	90	50	4	650	205	197	-8	30	25.6	4.4
1		300	500	40	180	50	3	420	130	107	-23	30	25.6	4.4
1	1000		500		270	50	4	1240	20	017	-3	45	25.6	19.4
1		300	500	40	0	50	5	900	270	287	17	30	25.6	4 . 4
1		300	500	80	90	M16	2	650	12-11 10-11-11	197	-8	25	25.6	6
1		300	500	80	180	M16	2	355		107	-8	30	25.6	4.4
1	1000	300	500	80	270			1230	015	017	2	45	25.6	19.4
1		300	500	80	0	M16	2			287	2	15	25.6	-10.6
1		300	500	80	90	M14	2	640		197	-3	20	25.6	-5.6
1		300	500	80	180		1		165	107	-58	30	25.6	4.4
1		300	500	80	270		3	1230		017	2	45	25.6	19.4
1		300	500	80	0	M14	3	920	280		7	25	25.6	6
1		300	500	80	90	50	3	630		197	2	25	25.6	6
1		300	500	80	180	50	3	400		107	-13	30	25.6	4.4
1		300	500		270	50	4	1230	015	017	2	45	25.6	19.4
1	1000	300	500	80	0	50	3	900	270	287	13	20	25.6	-5-6

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1	1230	200	50	20	90	M16	2	740	230	189	-41	40	2.4	37.6
	1230				180			500						37.6
	1230				270			200				35		32.6
	1230			20				1040				30		27.6
	1230			20				730						
	1230											40		37.6
					180			500				40		37.6
	1230				270			200				40		37.6
	1230			20				1030				40		37.6
	1230			20			1	800	240	189	-51	40	2.4	37.6
	1230			20	180			500				35	2.4	32.6
1	1230	200	50	20	270	50C	2	1230	015	009	-6	40		37.6
1	1230	200	50	20	0							40		37.6
1	1230	200	50		90							40		37.6
	1230				180						-36			27.6
	1230				270							30		27.6
	1230			40				1220				40		37.6
	1230				90						-41	35		32.6
	1230				180	M1.4	1	500	150	109	-41	20	2 . 4	32.6
	1230					M 1 4	7	1220	150	099	-51	30		27.6
	1230				270		2	1230	015	009	-6			37.6
				40								40		37.6
	1230				90						-51			42.6
	1230				180		2	330	105	099	-6	40		37.6
	1230				270									•
	1230			40							-56	45		42.6
	1230			80	90			730				30		27.6
	1230		50	80	180			500			-51	20	2.4	17.6
	1230		50	80	270						9		2.4	37.6
	1230		50	80	0	M16	2	1030	315	279	-36			37.6
1	1230	200	50	80	90	M14	0							•
	1230			80	180	M14	0						2.4	•
1	1230	200	50	80	270	M14	3	1215	007	009	1	45	2.4	42.6
1	1230	200	50	80	0			1050			-46			42.6
1	1230	200	50	80	90			750			-46			37.6
1	1230	200	50	80	180			515			-58			17.6
	1230				270	50C	1	220	070	009				32.6
	1230			80	0						9	45	2.4	
							-	,	- 10	- 1 /		* -	201	4200
1	1230	200	200	20	90	M16	2	720	220	189	-31	45	9.4	35.6
							1	500	150	000	-51	45	0 - 4	35.6
1	1230	200	200	20	270	M16	2	1220	010	000	-1	30	0 4	33.6
	1230			20		M16	2	920	280		-1	30	9.4	
				20	90	M14	1	900	240	100	-51	4.0	0 4	20.6
1	1230	200	200		180	M14			150		-51	35	9.4	
i	1230		200	20	270	M14		1215				40		25.6
1		200	200	20	0	M14			275		1		9 • 4	30.6
1		200	200	20	90	50C		910		189	4	30 45	9 • 4	20.6
1	1230	200	200	20	180	50C					-51		9 • 4	35.6
	1230	200	200						280		179	40	9.4	30.6
1				20	270	50C		1215	007		1	30	9 • 4	20.6
1		200	200	20	0	50C			277		1	30	9 • 4	20.6
1		200	200	40	90	M16	1			189	-46	40	9 • 4	30.6
1	1230		200		180	M16			150		-51	40	9.4	30.6
1		200	200	40	270	M16		1220			-1	40	9.4	30.6
1	1230		200	40	0		2		277		1	35	9.4	25.6
1		200	200	40	90	M14		700		189	-21	30	9.4	20.6
1	1230		200	40	180		1		150		-51	40	9.4	30.6
1	1230		200	40	270	M14			007	009	1	30	9.4	20.6
1	1230		200	40	0		2	1100	330	279	-51		9.4	
1	1230		200	40	90		1		225		-36	45	9.4	35.6
1	1230				180	50C			105		-6	40	9.4	30.6
1	1230	200	200	40	270	50C	3.	1215	007	009	Trian	-30	9.4	20.6
						12	TH	HIE	t it		Line	المالية	LI LIZE	A-16
						-	7 1	IDE	4171	44	The section of parameters	ng seriesco in management.		1

0.0	1	241	M.	LIV.	44
					称

UNGLASSILL

												OL.	DIED TO COL	
1	1230	200	200	40	0	50C	2	915	277	279	1	30	9.4	20.6
î				80		M16				189		40		30.6
1					180	M16				10,		10	9.4	•
1	1230				270			100	030	009	-21	60	9.4	50.6
1	1230			80	0			1045			-33	50		40.6
1	1230			80	90	M14		800			-51	40	9.4	30.6
1					180	M14			165		-66	50	9.4	40.6
1					270			1215			1	45		35.6
	1230			80	0			1030			-36	55	-	45.6
	1230			80				745			-43	45		35.6
	1230				180			500			-51	50		45.6
	1230				270			1215			1			
1	1230			80	0	50C	2	900	270	279	9	30		20.6
							_	,		_ , ,	,	-	,	2000
1	1230	200	500	20	90	M16	1	800	240	189	-51	45	22.4	22.6
	1230				180			445			-43		22.4	22.6
	1230				270			1230			-6		22.4	22.6
	1230			20	0			1030			-36		22.4	37.6
1	1230	200	500	20	90			900			-81		22.4	22.6
1	1230	200	500	20	180			330			-6	45	22.4	22.6
1	1230	200	500	20	270			1215			1		22.4	22.6
1	1230	200	500	20	0	M14				279	1		22.4	17.6
1	1230	200	500	20	90			300			99		22.4	32.6
1	1230			20	180	50C					-178		22.4	22.6
1	1230	200	500	20	270	50C	3	1230			-6		22.4	22.6
1	1230	200	500	20	0	50C	3	915	277	279	1		22.4	17.6
1	1230	200	500	40	90	M16	1	745	232	189	-43		22.4	12.6
1	1230			40	180	M16	1	500	150	099	-51		22.4	
1	1230			40	270			1245			-13		22.4	27.6
1	1230			40	0			1100			-51	45	22.4	22.6
	1230			40	90			800			-51	40	22.4	17.6
	1230				180	M1.4				099	-51	40	22.4	17.6
	1230				270			1215			1		22.4	22.6
	1230			40	0	M14		1045			-43		22.4	37.6
	1230			40	90	50C			195		-6		22.4	7.6
1	1230				180	50C				099	-13		22.4	22.6
1	1230				270			1230			-6		22.4	22.6
1	1230			40	0	50C					9		22.4	12.6
	1230			80	90	M16				189	-51		22.4	22.6
					180			500					22.4	
	1230			80	270	M16				009	-51		22.4	
	1230				0	M16					-36		22.4	37.6
1	1230			80	90	M14			240		-51		22.4	7.6
1	1230			80	180	M14			112		-13		22.4	17.6
1	1230			80	270			1215			1		22.4	22.6
1	1230			80	0	M14			277		1		22.4	7.6
1	1230			80	90	50C			217		-28		22.4	7.6
1	1230 1230				180	50C			144		-45		22.4	27.6
1	1230				270			1215			1		22.4	27.6
1	1230	200	300	80	0	50C	9	900	270	219	9	30	22.4	7.6
1	1200	300	50	20	90	M16	0			194			2 2	
i	1200		50		180	M16		500	150	VOII	-46	30	2.3	27 7
î	1200		50		270	M16			060		-46	30	2.3	27.7
1	1200		50	20	0	M16		1100			-46	30	2.3	27.7 27.7
1	1200		50	20	90	M14			240		-46	45	2.3	42.7
1	1200		50		180	M14		000	_ ,0	- / -	10	70	2.3	7201
1	1200		50		270	M14		215	67	014-	53.	45	2.3	42.7
1	1200		50	20	0			1100			14467	130	2.3	27.7
						130	4	HALL	打	4	UNTL.	NOS.	I Line 1	A-17
						00	1		DIA	L	man I change by Country Species of	1 re-vises-report		A-1 /

CONER	CHIEN!
WE THAT IS	ALL LANGE

CINCLESSAME:

			I Fre	[[F110] 1337F137]				EDNEWNTA				CI	ICIAS:	
				d Walani L	00.1.	i a .				V		HEL YOU LANGUE SOL	party , sales resided as a service.	der could be distributed.
1	1200		50	20		50C	1	800	240		-46	42	2.3	39.7
1	1200		50	20	180	50C		12/5		104			2.3	•
1	1200	300	50	20		50C	1	1245				30	2.3	27.7
1	1200		50	40	90	M16		1115	221	194	-53	30	2.3	27.7
1	1200		50	40	180	M16	1		150		-46	30	2.3	27.7
1			50	40		M16				014	6	35	2.3	32.7
1	1200	300	50	40	0	M16	1	1100			-46	30	2.3	27.7
1		300	50	40	90	M14	1			194			2.3	•
1	1200		50	40	180	M14	3	630			-1	75	2.3	72.7
1	1200		50	40				1230			-1	30	2.3	27.7
1	1200 1200	300	50	40	0	M14			255		29	45	2.3	42.7
1	1200		50 50	40	90 180	50C	1	530	247	194	-53	40	2.3	37.7
1	1200		50	40	270	50C		1245		104	-61 -8	30	2.3	27.7
1	1200		50	40	0		1	1115			-53	40	2.3	27.7 37.7
1	1200		50	80	90	M16			240	194	-46	30	2.3	27.7
1	1200	300	50	80	180	M16				104			2.3	
1	1200		50	80	270	M16				014			2.3	•
1	1200		50	80	0	M16				284			2.3	•
1	1200		50	80	90	M14		800	240		-46	30	2.3	27.7
1	1200 1200		50	80	180	M14		215	017	104			2.3	•
1	1200		50	80	270	M14	1	215	067		-53	40	2.3	37.7
1	1200		50	80	90	50C		815	247	284	-53	30	2.3	27 7
ī	1200		50	80		50C		013	241	104	-))	30	2.3	27.7
1	1200		50		270	50C	1	215	067		-53	30	2.3	27.7
1	1200	300	50	80	0	50C		1100		284	-46	40	2.3	37.7
1	1200		200	20	90		1	745	232		-38	40	9.2	30.8
1	1200		200	20	180	M16				104			9.2	•
1		300	200	20	2 7 0	M16				014			9.2	•
1		300	200	20	90	M14				284 194			9.2	•
1		300	200	20	180	M14	1	345	112	104	-8	40	9.2	30.8
1	1200	300	200	20	270	M14	1	145	52		-38	45	9.2	35.8
1	1200		200	20	0	M14		300	090	284	-166	15	9.2	5.8
1	1200			20	90	50C			240	194	-46	45	9.2	35.8
-	1200				180	50C				104			9.2	•
1	1200 1200	300	200		270	50C		020	205	014			9.2	•
1		300	200	20 40	90	50C M16		930	285	284	-1	30	9 • 2	27.8
1		300	200	40	180	M16				194			9 • 2	•
1	1200	300	200	40	270	M16				014			•	•
1	1200	300	200	40	0	M16		1100	330		-46	40	9.2	37.8
1	1200	300	200	40	90		1		225	194	-31	40	9.2	37.8
1		300	200	40	180	M14				104			9.2	•
1		300	200	40	270	M14							9.2	
1		300 300	200	40	90	M14		000	24.0	104		, ,	•	05 0
1		300	200	40	180	50C	1	800	240	194	-46	45	9.2	35.8
i	1200	300	200		270		1	215	075		-61	40	9.2	30.8
1		300	200	40	0		1		105		179	30	9.2	20.8
1	1200	300	200	80	90	M16	0			_ • •		20	9.2	
1	1200	300	200		180	M16	0						9.2	
1	1200	300	200		270		1		060		-46	30	9.2	20.8
1	1200	300	200	80	0		1	1230	015	284	-91	45	9.2	35.8
1		300	200	80	90	M14			100	10.			9.2	•
1		300	200		180 270	M14 M14		400	120	104	-16	30	9.2	20.8
•	2200	500	200	00	210		M	PE IA	417	- D.	UNGL		9.2	A-18
						4	04	TITO	-11	11	MARCO - M. ABO 44 - MAR. M. ARL.	es	-	A-10

											and the second	rest surtainment of the	arandados (1800, July 19 Junio	. ,
						ę	V	胜格	渊	州		GLA	SSHIE	4
1	1200	300	200	80	0	M14	1	1100	330	284	-46	45	9.2	35.8
1	1200	300	200	80	90	50C	0						9.2	
1	1200	300	200	80	180	50C	1	400	120	104	-16	30	9.2	20.8
1	1200	300	200	80	270	50C	1	330	105	014	-91	40	9.2	30.8
1	1200	300	200	80	0	50C	1	1000	300	284	-16	60	9.2	50.8
1	1200	300	500	20	90	M16	0						22.0	
î	1200	300	500	20	180	M16	1	500	150	104	-46	40	22.0	1.0
1	1200	300	500	20	270	M16	1	215		014	-53	30	22.0	18.
1	1200	300	500	20	0	M16	î	1100	330	284	-46		22.0	33.
1	1200	300	500	20	90	M14	1	815	247		-53	45		23.
1	1200	300	500	20	180	M14	2	400	120	104	-16	45	22.0	23.
1	1200	300	500	20	270	M14	1	1245		014	-8	40	22.0	18.
1	1200	300	500	20	0	M14	1	130	045	284	-121	45	22.0	23.
1	1200	300	500	20	90	50C	2	645	202	194	-8	40	22.0	18.
1	1200	300	500	20	180	50C	1	500	150	104	-46		22.0	23.
1	1200	300	500	20	270	50C	2	1245	022	014	-8		22.0	23.
1	1200	300	500	20	0	50C	3	530	165	284	119		22.0	8.
1	1200	300	500	40	90	M16							22.0	•
1	1200		500	40	180	M16							22.0	•
1	1200	300	500	40	270	M16							22.0	
1	1200	300	500	40	0	M16							22.0	•
1	1200	300	500	40	90	M14							22.0	•
1	1200	300	500	40	180	M14							22.0	•
1	1200	300	500	40	270	M14							22.0	•
1	1200	300	500	40	0	M14							22.0	•
1	1200	300 300	500	40	90	50C							22.0	•
1	1200		500	40	180 270	50C							22.0	•
i	1200		500	40	0	50C							22.0	•
î	1200	300		80	90		1	700	210	104	-16	4.0	22.0	1.0
ī	1200		500	80	180	M16	i	400	120	104	-16		22.0	18.
1	1200		500	80	270	M16	2	1215	007	014	6	45	22.0	23.
1	1200		500	80	0	M16	2	900	270	284	14	30	22.0	8.
1	1200	300		80	90	M14	2	615	187	194	6	30	22.0	8.
1	1200	300		80	180	M14	2	400	120	104	-16	-	22.0	18.
1	1200	300	500	80	270	M14	1	315	097	014	-83	40	22.0	18.
1	1200	300	500	80	0	M14	2	1200	000	284	-74		22.0	48.
1	1200	300	500	80	90	50C	3	645	202	194	-8		22.0	18.
1	1200	300	500	80	180	50C	1	515	157	104	-53		22.0	23.
1	1200	300	500	80	270	50C	3	1230	015	014	-1	45	22.0	23.
1	1200	300	500	80	0	50C	3	900	270	284	14		22.0	23.



CONCIDENTAL PROPERTY.

										i.	Mary Corting and constitution to control	M terminals . a.a.		
1	1400	200	50	20	90	M16	0			188			2.0	
1	1400		50		180	M16				98			2.0	
1	1400	200	50	20		M16				008			2.0	
1	1400	200	50	20	0	M16			315		-37	5		
1	1400		50	20	90	M14	1		240		-52	65	2.0	63.
1	1400		50	20	180	M14	1	300	90	98	8	80	2.0	78.
1	1400		50	20	270	M14	1	200	60	8	-52 -47	0	2.0	-2.
1	1400		50	20	0	M14	1	1050	325	278	-47	0	2.0	-2.
1	1400		50	20	90	50	0			188			2.0	
1	1400		50		180					98			2.0	
1	1400		50		270			220			-62		2.0	
1	1400 1400		50 50	20	0			1100				30	2.0	
1	1400		50	40	90	M16		740			-72	30	2.0	28.
1	1400		50		270			140			-42	20	2 0	•
1	1400		50	40	0			1020			-32	20 35	2.0	18. 33.
1	1400		50	40	90	M14			240		-52	30	2.0	
1	1400		50		180	M14					-52	25	2.0	23.
1	1400		50		270	M14			60	8	-52	20	2.0	18.
1	1400	200	50	40	0	M14			150		128	75	2.0	73.
1	1400		50	40	90	50	1	820	250		-62	30	2.0	28.
1	1400		50	40	180	50	2	320	100	98	-2	30	2.0	28.
1	1400		50		270	50	2	1220	10	8	-2	30	2.0	28.
1	1400		50	40	0	50						30	2.0	28.
1	1400		50	80	90			740			-72		2.0	23.
1	1400		50		180	M16							•	•
1	1400		50	80	270	M16			45		-37		2.0	
1	1400 1400		50 50	80	90			1030			-37	30	2.0	28.
1	1400		50		18.0	M14		750 450			-77 -77	25	2.0	23.
1	1400		50	80	270				10	8		35	2.0	13. 33.
i	1400		50	80	0			1040				35	2.0	33.
	1400		50	80		50	2	800	240	188		30		28.
	1400		50		180	50	1	800 500	150	98	-52		2.0	
	1400		50		270	50	2	1215			0	30		
1	1400	200	50	80	0	50	2	910			3			-2.
	1400			20	90	M16			235		-48	30	8.0	
	1400		200		180	M16				98	-52	30	8.0	22.
1	1400 1400		200		270			1240	20	8	-12	50	8.0	42.
1	1400		200	20	90	M14		750	320	188	-42 -47	50	8.0	42.
1	1400	200	200	20	180	M14	2	500	150	98	-52	45	8.0	37·
1	1400	200	200	20	270	M14	2	200	60	8	-52	45	8.0	37.
1	1400	200	200	20	0	M14	2	1010	305	278	-27	15	8.0	7.
1	1400	200	200	20	90	50	2	800	240	188	-52	40	8.0	32.
1	1400	200	200	20	180	50	3	520	160	98	-62	40	8.0	32.
1	1400	200	200	20	270	50	3	1240	20	8	-12	25	8.0	17.
1		200	200	20	0	50	3		330	278	-52	40	8.0	32.
1		200	200	40	90	M16	1		232	188	-44	25	8.0	17.
1	1400	200	200	40	180	M16	1	450	140	98	-42	30	8.0	22.
1	1400	200	200	40	270	M16	1	200	60	8	-52	20	8.0	12.
1	1400	200	200	40	90	M16 M14	2	800	320	278	-42	0	8.0	-8.
1	1400	200	200	40	180	M14	4	330	240 105	188	-52 -7	30	8.0	22.
1	1400	200	200	40	270	M14	2	120	40	8	-32	55	8.0	27· 47·
1	1400	200	200	40	0	M14	5		300	278	-22	50	8.0	42.
1	1400	200	200	40	90	50	2		240	188	-52	35	8.0	27.
1	1400	200	200	40	180	50	3	330	105	98	7			22.
1	1400	200	200	40	270	50	3.	1220	120	8	742	25	8.0	17.
						-63		其其	#31	AL	Out Les	10011	112-6	A-20
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BONETS	DEED
CONTINUE	THE DOL

UNGLASSIFIER

1	1400	200	200	40	0	50	2	1020	310	278	-32	45	8.0	37.
1	1400	200	200	80	90	M16	1	840	260	188	-72	25	8.0	17.
1	1400	200	200	80	180	M16	1	500	150	98	-52	20	8.0	12.
1	1400	200	200	80	270	M16		1220	10	8	-2	30	8.0	22.
1	1400		200	80	0	M16	1	1020	310		-32	50	8.0	42.
1	1400	200	200	80	90	M14	2	820	250	188	-62	30	8.0	22.
ì	1400	200	200	80	180	M14	1	500	150	98	-52	20	8.0	12.
î		200	200	80	270	M14	3	1220	10	8	-2	35	8.0	27.
1		200	200	80	0	M14	1	1030	315	278	-37	50	8.0	42.
1	1400		200	80	90	50	2	740	230	188	-42	40	8.0	32.
1	1400	200		80	180	50	3	340	110	98	-12	30	8.0	22.
1	1400				270	50	3	200	60	8	-52	40	8.0	32.
1	1400			80	0		3	900	270		8	30	8.0	22.
1	1400	200	200	00	O	50	2	900	210	210	0	30	0.0	220
1	1400	200	500	20	90	M16	1	740	230	188	-42	40	19.4	20.6
î		200	500	20	180	M16		140	200	98	72	40	19.4	20.0
1	1400	200	500	20	270	M16	1	210	65	8	-57	40	19.4	20.6
1	1400		500	20	0	M16	1	1000	300	278	-22	45	19.4	25.6
1	1400	200	500	20	90	M14	2	650	205	188	-17	45	19.4	25.6
1	1400	200	500	20	180	M14	1	540	170	98	-72	35	19.4	15.6
1	1400	200	500	20	270	M14	1	200	60	8	-52	55	19.4	35.6
1	1400	200	500	20	0	M14	4	920	280		-2	0	20 10 10 10 10 10 10 10 10 10 10 10 10 10	-19.4
1	1400	200	500	20	90	50	3	640	200	188	-12	30	19.4	10.6
	1400		500					500					19.4	
1	1400	200	500	20	180	50	2		150	98	-52 -2	55	19.4	35.6 10.6
1	1400	200	500	20	270	50 50	4	910	10 275	278	3	30		
1.		200	500	40	90	M16	1	800	240	188	-52	15 35	19.4	-4.4
1	1400	200	500	40	180	M16	1	525	162	98	-64	35	19.4	15.6 15.6
1	1400	200	500	40	270	M16	1	150	55	8	-47	50	19.4	30.6
1	1400	200	500	40	0	M16	1		310	278	-32	40	19.4	20.6
1	1400	200	500	40	90	M14	1	750	235	188	-47	35	19.4	15.6
1	1400	200	500	40	180	M14	1	550	175	98	-77	40	19.4	20.6
1	1400	200	500	40	270	M14	1	210	65	8	-57	60	19.4	40.6
1	1400	200	500	40	0	M14	1	1050	325	278	-47	50	19.4	30.6
1	1400	200	500	40	90	50	2	640	200	188	-12	30	19.4	10.6
1	1400	200	500	40	180	50	2	500	150	98	-52	50	19.4	30.6
1	1400	200	500	40	270	50	3	1230	15	8	-7	35	19.4	15.6
1	1400	200	500	40	0	50	2	950	295	278	-23	30	19.4	10.6
1	1400	200	500	80	90	M16	1	730	225	188	-37	35	19.4	15.6
1	1400	200	500	80		M16		350	115	98	-17	30	19.4	
1	1400	200	500	80	180	M16		1220	10	8	-17	45	19.4	10.6
-	1400							940						25.6
1		The second of		80	0						-12 -27		19.4	
1	1400			80	90	M14			215				19.4	• 6
1	1400				180	M14		500	150	98	-52		19.4	10.6
1	1400				270	M14		1220	10	8	-2			25.6
1	1400			80	0	M14			280		-2	35	19.4	15.6
1	1400		500	80	90	50	2	620	190	188	-2	15	19.4	-4.4
1	1400		500		180	50		340	110	98	-12	30	19.4	10.6
1	1400				270			1220	10	8	-2		19.4	25.6
1	1400	200	500	80	0	50	2	830	255	278	23	30	19.4	10.6

(SPECIAL TEST DATA

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						1	H	出量	W	数	THE	PIS	SSIFIE	17
	F 0 0	200	005			147.4	,				101		O HA HE	42.3
. M		300			090	M14	1		067		135	45		
M	500	55	025	020	180	M14	3	330	105	112	7	15	2.7	12.3
M	500	300	025	020	270	M14	2	1245		022	0	15	2.7	12.3
M		300	025	020	000	M14	2	945	292	292	0	15	2 .	12.3
M		300	050	020	090	M14	1		247		-45	45	5.3	
M	500	300	050	020	180	M14	2	345	112	112	0	30	5.3	24.7
M	500	300	050	020	270	M14	2	100		022	-8	15	5.3	9.7
M	500	300	050	020	000	M14	3	945	292		0	0	5.3	-5.3
M	500	300	075	020	090	M14	2	830	255	202	-53	45	7.6	37.4
14	500	300	075	020	180	M14	3	400	120	112	-8	30	7.6	22.4
M	500	300	075	020	270	M14	3	100	030	022	-8	30	7.6	22.4
M	500	300	075	020	000	M14	3			292		90	7.6	82.4
M	500	300	100	020	090	M14	2	800	240	202	-38	45	10.1	34.9
M	500	300	100	020	180	M14	3	400	120	112	-8	30	10.1	19.9
M		200	100	020	270	M14	3	100	030	022	-8	30	10.1	19.9
M	500	300	100	020	000	M14	3	1000	330	292	-38	15	10.1	4.9
M	50C	300	150	020	090	M14	2	745	232	202	-30	45	15.2	29.8
M		300	150	020	180	M14	3	400	120	112	-8	30	15.2	14.8
M		300	150	020	270	M14	3	115	037	022	-15	40	15.2	24.8
M		300	150	020	000	M14	2	945	292	292	0	30	15.2	14.8
M	2000 2000 2000	300	200	020	090	M14	3	700	210	202	-8	40	20.3	19.7
M		200	200	020	180	M14	3	400	120	112	-8		20.3	9.7
M		300		020	270	M14	3	1215	007	022	15	0	20.3	-20.3
M		300	200	020	000	M14	3	945	292	292	0	30	20.3	9.7
M	500	300	300	020	090	M14	3	700	210	202	-8	40	31.0	9.0
M		300	300	020	180	M14	3	415	127	112	-15	50	31.0	19.0
M		200	300	020	270	M14	3	100	030	022	-8	45	31.0	14.0
M		300	300	020	000	M14	2	930	285	292	13	30	31.0	-1.0
M		300	500	020	090	M14	2	700	210	202	-8	40	42.8	-2.8
M		300	500	020	180	M14	3	430	135	112	-13	50	42.8	7.2
M		200	500	020	270	M14	3	100	030	022	-8		42.8	17.2
M		300	500	020	000	M14	2	945	292		0	30	42.8	-12.8
N						•							•	•
0	1000	100	200	080	090	M16	1	830	255	186	-69	.0	11.3	-11.3
0	1000	100	200	080	180	M16	1	800	240	096	-144	0	11.3	-11.3
0	1000	100	200	080	270	M16	3	1200	360	006	6	40	11.3	28.7
0	1000	100	200	080	000	M16	3	900	270	276	6	40	11.3	28.7
0	1000	100	200	080	090	MI	2	640	200	186	-14	0	11.3	-11.3
Ö	1000	100	200	080	180	MI	3	330	105	096	-9	25	11.3	13.7
O	1000	100		080	270	M1	4	1215		006	-1	40	11.3	28.7
C	1000	100	200	080	000		2			276	6	30	11.3	18.7
0	1000	100	200	080	090	M14	1	720	220	186	-34	45	11.3	33.7
0	1000	100	200	080	180	M14	3	330	105	096	-9	30	11.3	18.7
0	1000	100	200	080	270	M14	3	1220	010	006	-4	40	11.3	28.7
0	1000	100	200	080	000	M14	2	900	270	276	6	50	11.3	38.7
0	1000	100	200	100	090	M14	2	700	210	186	-24	45	11.3	33.7
0	1000	100	200	100	180	M14	2	330	105	096	-9	30	11.3	18.7
0	1000	100	200	100	270	M14	2	1215	007	006	-1	40	11.3	28.7
0	1000	100	200	100	000	M14	2	900	270	276	6	60	11.3	48.7
0	1000	100	050	100	090	M14	2	730	225	186	-39	50	2.9	47.1
0	1000	100	050	100	180	M14	2	500	150	096	-54	10	2.9	7 • 1
0	1000	100	050	100	270	M14	3	1210	005	006	1	40	2.9	37.1
0	1000	100	050	100	000	M14	2	900	270	276	6	70	2.9	67.1
0	1000	100	050	080	690	M14	2	740	230	186	-44	30	2.9	27.1
O	1000	100	050	080	180	M14	2	500	150	096	-54	15	2.9	12.1
0	1000	100	050	080	275	1414	1	200	060	006	-54	45	2.9	42.1
0	1000	100	050	080	000	M14	2	1030	315	276	-39			
0	1000	100	500	080	090	1414	2		190	186	-4	10	26.5	-16.5
0	1000	100	500	080	180	1414	2	350	115	096	-19		•	•
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()	1000	100	500	080	000	1414	2	850	265		II			
0		100		100		M14	1	730	235	186	-49	50	26.5	23.5
0	1000		_		180	3414]	515	157		-61	40	26.5	13.5
0	1000		500	100		M14	1		060		-54	30	26.5	3.5
0	1000		500	100		M14	2	815	247		29	45	26.5	18.5 33.7
0	1000	100	200	080	0 90	M60	3	645 745	202		-16 -136	60	11.3	48.7
0	1000			080	270	M60	3	1230	015	006	-9	40	11.3	28.7
0	1000		200		180	M60	2	445		276	134	30	11.3	18.7
0	1000		200		090	M60	5	700		186	-24	45	11.3	33.7
C	1000	100	200	080	000	M60	9	900	270	096	-174	60	11.3	48.7
()	1000	100	200	080	270	M60	1	1230	015	006	-9	30	11.3	18.7
0		100	200	080	180	M60		200		276	144	45	11.3	33.7
0	1000		200		090	50C		1200	360		-174	0		-11.3
0		100		080	000	500		900			-174	35	11.3	23.7
0	1000		200					1215		006	-1		11.3	18.7
0	1000		200		180	50C	3	315		276	179	25	11.3	13.7
0		100			090	50C		1145 845			-166	20	11.3	8 • 7 28 • 7
0		100	200		270	50C		1245		006	-166 -16	40	11.3	28.7
0	1000			080	180	50C		315			179	30	11.3	18.7
0		100			090	K56		710	215		-29	20	11.3	8.7
0	1000		200	080	000	K56	3	900			-174	30	11.3	18.7
0		100	200		270	K56		115	037		-29	45	11.3	33.7
0	1000	100	200		180	K56	1	400		276	156	15	11.3	3.7
C	1000	100	200	080	090	762	1	700	210	186	-24	40	11.3	28.7
O	1000	100	200	080	000	762	2	250	085	096	11	35	11.3	23.7
C	1000		200	080	270	762	4	130	045	006	-39	35	11.3	23.7
0	1000	-	200	080	180	762	3	315	(197			25	11.3	13.7
0	1000		200		990	125	2	700	210	186	-24	45	11.3	33.7
0	1000		200		000	125	3				-174	35	11.3	23.7
0	1000		200		270	125		1230	015		134	35 25	11.3	23.7
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Ü	1000		200	080	000	20M	3	245		096	14	30	11.3	18.7
O	1010	100	200		270	20M		1245		006	-14	35	11.3	23.7
0	1000		200	080	180	20M	3	330			171	25	11.3	13.7
0	1000	100	200	080	099			1150	355	186	-169	15	11.3	3.7
0	1000	100	200	080	000	23M	3	855	261	096	-171	35	11.3	23.7
0	1000			080		23M		1230		006	-9	35	11.3	23.7
C	1000					23N					179	20		
0		200		080		SUC			225	190	-35	30	9.4	20.6
0	1200		200	080	.00	50C		930	285	280	-5	15	9.4	5.6
0	1200		200	080		500		1245	022		-12	30	9.4	20.6
0	1200 1200	200	200	080	180	50C K56	1	500 710	150 215	100	-50 -25	15	9.4	5.6
0	1200		200	080	000	K56		930	285	280	-25	45	9.4	35.6
0	1200		200	080	270	K56		1215	007		2	45	9.4	35.6
0	1230		200	080	180	K56	1	425		100	-32	60	9.4	50.6
0	1200		200	080	090	762	2	700	210	190	-20	0	2.4	-9.4
0	1200		200	080		762	4	800	240	280	40	15	9.4	5.6
0	1200	200	200		270	762			0.30		-20	30	9.4	20.6
0		200	200	080	180	762	1	445	142	100	-42	15	9.4	5.6
C	1200		200		J90	125	2	730	225	190	-35	30	0.4	20.6
0	1200		20	080	000	125	2	900			10	60	9.4	50.6
C	1200		20.	080	270	125	3	1250	025	010	-15	30	9.4	20.6
0	1200		200	080	180	125	2	445	142	100	-42	25	9.4	15.6
0	1400		200	080	093	M16		0/:=	202	188	-14	50	0.8	420
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0	1400	200	200	080	090	M1.			225	188	-37	20	13		-	
0	1400	200	200	080	000	M1				278		0				
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0	1400	200		080		MI						15		7.0		
0	1400	200			090	M14						15				
0	1400	200			000	M14				278		60				
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0	14 10	200		080		M14						15				
0	1400	200	200	080	090	M60			212			30				
0	1400	200	200	080	000	M60					-7	50				
0				080	270	M60					-112	40				
0			200	080	160	M60	1	430		098		15				
0	1400	200	200	080	090	50C	2	730	225	188	-37	35				
0				080	000	50C	3	900	270	278	8	0				
0						50C	2	1245	022	008	-14	30	8.0			
0	1400	200	200	080		50C			210	098	-112	20	8.0			
0	1400	_								188			8.0			
0	1400			080		K56			270	278	8	45	8.0			
0	1400			080		K56			030		-22	30	8.0	22.0		
0	1400			080	180	K56			127	098	-129	15	8.0	7.0		
0	1400			080		762			210	188	-22		8.0	•		
0	1400		200			762			270	278	8	0	8.0	-8.0		
0	1400				270	762				800	-17	30	8.0	22.0		
0	1400				180	762					-37	0	8.0	-8.0		
0	1400			080	090	125			225	188	-37	35	8.0	27.0		
0	1400				000		2		270	278	. 8	45	8.0	37.0		
0	1400	1		080	270	125	3			800	-7	30	8.0	22.0		
0	1400			080	180	125		445		098	-52	15	8.0	7.0		
0	1400	200		080		23M				188	-37	15	8.0	7.0		
0	1400	200		080		23M				278	8	0	8.0	-8.0		
0	1400				270	23M		1230		800	-7	30	8.0	22.0		
P	1400	200	200	080	180	23M	2	315	097	098	1	20	8 • 0	12.0		
Q	500	200	200	080	000	M14	2	(20	104	200	-		•	•		
Q			200		180	M14	3	400	195	112	7	10		-10.3		
Q	500		200		270			1230		022	-8 7	35	20.3	9.7		
Q	500	200	200	080	000	M14				292	22		20.3			
0	500	200	200		090		1		190		12	15				
Q	500	200		080	180	M14			125	112	-13		20.3			
Q				080				1240						-·3 -14·7		
Q	500	200	200	080	000		2		290		2	30		-9.7		
R	1000	100	200	020	090	50C		,	_ , 0	188	2	50	11.3	-9.1		
R	1000	100	200	020	270	50C	3			008			11.3	•		
R	1000	100	200	020	090		1	700	210	188	-22	30	11.3	18.7		
R	1000	100	200	020	270	50C	3		- 0	008		20	11.3	1007		
R	1000	100	200	020	090	50C		615	187	188	1	30	11.3	18.7		
R	1000	100	200	.020	270	50C	3			008	_	30	11.3	1001		
R	1000	100	200	020	090		0			188			11.3			
R	1000	100	200	020	270	50C	3			008			11.3			
R	1000	100	200	020	090	M60	0			188			11.3			
R	1000	100	200	020	270	M60	1	1220	010	800	-2	30	11.3	18.7		
R	1000	100	200	020	090	M60	0			188		A-	11.3	•		
R	1000	100	200	020	270	M60	1	1230	015	800	-7	30	11.3	18.7		
R	1000	100	200	020	090	M60	0			188			11.3	•		
R	1000	100	200	020	270		2	1230	015	800	-7	20	11.3	8.7		
R	1000	100	200	020	090		0			188			11.3	•		
R	1000	100	200	020	270	M60	2	1230	015	800	-7	20	11.3	8.7		
S	600	200	050	0.5.5	0.00								•	•		
T	500	300	050	020	090	M14	1			211	T	/ ====	4.9			
Offic Three Las									UNI	LASSI						
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T	The state of the s	300	050		180	M14		400	120	121	1	30	4.9	25.1
Ţ		300	050	100	270	M14		115	037		-6	35	4.9	30.1
T		300	050	020	000	M14			295		-54	15	4.9	10.1
T		300	050		180	50C	2	850 400	265		-54 1	30 30		25.1 25.1
Ť		300	050	020	270	500	2	100	1	031	1	35	4.9	30.1
T		300	050	020	000	50C	2	950	295		6	5	4.9	• 1
T	500	300	050	080	090	M14		700	210		1	10	469	5.1
T		300	050	080	180	M14	1	515	157		-36	10	4.9	5.1
T		300	050	080	270	M14	2	100	030		1	30	4.9	25.1
T		300	050	080	000	M14		1000	300		1	25	4.9	20.1
T		300	050	080	090	50C	2	700	210		1	10	4.9	5.1
T		300	050	080	180	50C		400	120	121	1	20	4.9	15.1
T		300	050	080	270	50C	1 2	230		031	-44	30	4.9	25.1
T		300	200	020	090	M14	3	700	300 210		1	20 35	4.9	15.1 16.0
T		300	200	020	180	M14		400	120	121	1	60	19.0	41.0
T	500	300	200	020	270	M14	3	1210	005		26	20	19.0	1.0
T	500	300	200	020	000	M14	3	950	295		6	30	19.0	11.0
T		300	200	020	090	50C	1	730	225	211	-14	35	19.0	16.0
Ţ		300	200	020	180	50C	2	330	105	121	16	35	19.0	16.0
T		30C	200	020	270	50C	2	115	037		-6	35	19.0	16.0
T		300 300	200	080	090	50C M14	2	940	290	301	11	30	19.0	11.0
Ť		300	200	080	180	M14	2	650 430	205 135	211	-14	20	19.0	1.0
T		300	200	080	270	M14	2	110	035		-4	40	19.0	21.0
T	500	300	200	080	000	M14	3	940	290	301	11	30	19.0	11.0
T	500	300	200	080	090	50C	2	650	205		6	20	19.0	1.0
T		300	200	080	180	50C	2	410	125	121	-4	25	19.0	6.0
T	1.02	300	200	080	270	50C	2	110	035	031	-4	40	19.0	21.0
T		300	200	080	000	50C	2	930	285	301	16	30	19.0	11.0
T		300 300	200	080	090	K56	2	700	210	211	1	30	19.0	11.0
T		300	200	080	270	K56	3	400	120	121	1 -4	25 30	19.0	6.0
T		300	200	080	000	K56	1	330	105	301	-164	30	19.0	11.0
T	1000	300	050	020	390	M14	1	815	247		-50	30	2.7	27.3
T		300	050	020	180	M14	1	500	150	107	-43	30	2.7	27.3
T		300	050	020	270	M14	2	215	067	017	-50	30	2.7	27.3
Ţ		300	050	020	000	M14	4	340	110	287	177	0	2.7	-2.7
T	THE COME OF SALE	300	050	020	090	50C	1	815	247		-50	30	2.7	27.3
T						50C			150		-43	30	2.7	27.3
T						50C		920	280		-52 7	15	2.7	12.3
T					090	M14	1	800			-43	15	2.7	12.3
T						M14	1	500		107	-43	5	2.7	2.3
T	1000		050	080	270	M14	2	1245	022	017	-5	20	2.7	17.3
Т	1000			080		M14		700		287	77	35	2.7	32.3
T	1000			080		50C		800		197	-43	15	2.7	12.3
T	1000			080		50C			150		-43	10	2.7	7.3
T	1000			080		50C		1230	330		2	30	2.7	27.3
T	1000			020		M14		800		197	-43 -43	35	2.7	32.3
T				020		M14		330		107	2	3()	10.9	19.1
T	1000		200		270	M14		230	075		-58		10.9	29.1
T	1000			020		M14	2	915	277	287	10	10	10.9	9
T	1000			020		50C		620		197	7		10.9	24.1
T	1000				180	50C				107	-13		10.9	14.1
T				020		50C		130	045		-28		10.9	59.1
T				080		M14		920 730		287 197	7 -28		10.9	9 29.1
100							-	0						
							H	HH	HH	住田		GLAS	SIFE	9 (
												and constraint in some	Marie Marie Marie Annual	A-26

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	1000	300	200	0.80	180	M14	Y	340			-3	25	10.9	1461
						M14		1250	025		-8		10.9	19.1
	1000			080	000	M14	3	930	285		2		10.9	19.1
	1000		200	080	Committee of the contract of	50C	1		232	197			10.9	19.1
			200	080	180	50C	2	350		107	-8		10.9	14.1
	1000		200	080	270	50C								
-							2		030		-13		10.9	
			200	080	000	50C	1	915		287	10		10.9	4.1
1			200	080	090	K47	2	710	215	197	-18		10.9	9
	1000		200	080	180	K47	2	400	120	107	-13		10.9	19.1
1			200	080		K47	3	145		017	-35	35	10.9	24.1
		-	200	080		K47	3	920		287	7		10.9	9
.]			50	020		M14	1	800	240		-46	100	2.3	27.7
1			50		000	M14		1100	330		-46		2.3	17.7
1			50	020		M14	1	200	060		-46	0	2.3	-2.3
1			50	020	180	M14	0			104			2.3	•
1		300	50			50C			247		-53		2.3	27.7
1			50		180	50C	1	515	157		-53		2.3	27.7
1			50		270	50C	2	645	202		72	45	2.3	42.7
1			50	020		50C	2	915		284	7	0	2.3	-2.3
1			50	080	090	M14	1	800	240	194	-46	30	2.3	27.7
1			50		000	M14		1100	330	284	-46		2.3	27.7
1			50		270	M14	1	200	060		-46		2.3	12.7
1			50	080	180	M14	1	530	165	104	-61	45	2.3	42.7
1			50	080	090	50C	1	815	247	194	-53	30	2.3	27.7
1			50	080	000	50C	2	1230			-91	30	2.3	27.7
1			50	080	270	50C	1	500	150	014	-136	0	2.3	-2.3
1			50	080	180	50C	2	915	277	104	-173	0	2.3	-2.3
1			200	020	090	M14	3	645	202	194	-8	15	9.2	5.8
1	1200	300	200	020	000	M14	4	915	277	284	7	0	9.2	-9.2
1			200	020	270	M14	4	1230	015	014	-1	30	9.2	20.8
1		300		020	180	M14	3	400	120	104	-16	30	9.2	20.8
1				020	090	50C	1	800	240	194	-46	40	9.2	30.8
1			200	020	000	50C	2	915	277	284	7	15	9.2	5.8
1			200	020	270	50C		1230	015	014	-1	30	9.2	20.8
1			200	020	180	50C	2	330	105	104	-1	15	9.2	5.8
1			200	080	090	M14	2	630	195	194	-1	0	9.2	-9.2
1			200	080	000	M14	3	330	105	284	-179	15	9.2	5.8
1		300	200	080	270	M14	3	1245	022	014	-8	30	9.2	20.8
1		300	200	080	180	M14	3	900	270	104	-166	15	9.2	5.8
1				080		50C	2	630	195	194	-1	15	9.2	5.8
T	1200	300	200	080	000	50C	2	330	105	284	-179	30	9.2	20.8
T	1200	300	200	080	270	50C	2	1230	015	014	- 1	30	9.2	20.8
T		300	200	080	180	50C	2	915	277		-173	15	9.2	5.8
T		300	50	020	090	M14	0			211			4.9	•
T		300			000	M14	1	1115	337	301	-36	10	4.9	5.1
T	500	300	50	020	270	M14	0			031			4.9	•
T	500	300	50	020	180	M14	2	400	120	121	1	30	4.9	25.1
T	500	300	50.	020	090	50C	1	820	250	211	-39	30	4.9	25.1
1	500	300	50	020	000	50C	2	1000	300	301	1	60	4.9	55.1
T		300		020	270	50C	2	100	030	031	1	30	4.9	25.1
T	500	300	50	020	180	50C	2	400	120	121	1	30	4.9	25.1
T	500	300	50	080	090	M14	2	700	210	211	1	15	4.9	10.1
T		300		080		M14		950	295	301	6	30	4.9	25.1
T		300	50	080	270		2	100	030	031	1	30	4.9	25.1
T		300	50	080	180	M14	2	400	120	121	1	15	4.9	10.1
T		300	50	080	090		2	700	210	211	1	20	4.9	15.1
T		300	50	080	000	50C	2	1000	300	301	. 1	25	4.9	20.1
T		300	50	080	270	50C		100	030		1	30	4.9	25.1
T	500	300	50	080	180	50C	2	400	120	121	1	20	4.9	15.1
T	500	300	200	020	090	M14	2	700	210	211	_ 1	30	19.0	11.0
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T	50 :	300	200	020	600	M14	3	450	145.		156	30	19.0	11.0
T	500	300	200	020	270	M14	4	115	037	031	-6	35	19.0	16.0
T	500	300	200	020	180	M14	5	400	120	121	1	30	19.0	11.0
T	500	300	200	020	090	50C	2	700	210	211	1	30	19.0	11.0
T	500	300	200	020	000	50C	2	950	295	301	6	30	19.0	11.0
T	500	300	200	020	270 180	50C	2	115	037	031	-6 11	20	19.0	11.0
T	500	300	200	080	090	M14	3	710	215	211	-4	20	19.0	1.0
Ť	500	300	200	080	000	M14	3	950	295	301	6	35	19.0	16.0
Ť	500	300	200	380	270	M14	4	100	030	031	1	40	19.0	21.0
T	500	300	200	080	180	M14	3	400	120	121	1	20	19.0	1.0
T	500	300	200	080	090	50C	2	700	210	211	1	20	19.0	1.0
T	500	300	200	080	000	50C	2	945	292	301	9	30	19.0	11.0
T	500	300	200	080	270	50C	2	1115	337	031	54	35	19.0	16.0
T	500	300	200	080	180	50C	2	415	127	121	-6	30	19.0	11.0
T	1000	300	50	020	090	M14	1	830	255	197	-58	30	2.7	27.3
T	1000	300	50	020	000	M14	1	1100	330	287	-43	30	2.7	27.3
T	1000	300	50	020	270	M14	3	1230	015	017	2	30	2.7	27.3
T	1000	300	50	020	180	M14	1	500	150	107	-43	30	2.7	27.3
T	1000	300	50	020	090	50C	1	820	250	197	-53	30	2.7	27.3
T	1000	300	50	020	270	50C	2	940 1240	290	287	-3 -3	10	2.7	7.3
T	1000	300	50	020	180	50C	1	500	150	107	-43	30	2.7	27.3
T	1000	300	50	080	090	M14	1	800	240	197	-43	25	2.7	22.3
Ť	1000	300	50	080	000	M14	3	920	280	287	7	40	2.7	37.3
T	1000	300	50	080	270	M14	2	1240	020	017	-3	30	2.7	27.3
T	1000	300	50	080	180	M14	2	330	105	107	2	30	2.7	27.3
T	1000	300	50	080	090	50C	1	800	240	197	-43	30	2.7	27.3
T	1000	300	50	080	000	50C	2	930	285	287	2	0	2.7	-2.7
T	1000	300	50	080	270	50C	1	220	070	017	-53	20	2.7	17.3
T	1000	300	50	080	180	50C	2	330	105	107	2	20	2.7	17.3
Ţ	1000	300	200	020	090	M14	2	800	240	197	-43	30	10.9	19.1
T	1000	300	200	020	000	M14	3	915	277	287	10	5	10.9	-5.9
T	1000	300	200	020	270 180	M14	4	1245 330	022	017	- 5	30	10.9	19.1
T	1000	300	200	020	090	50C	2	640	200	197	-3	30	10.9	19.1
T	1000	300	200	020	000	50C	2	420	130	287	157	10	10.9	9
T	1000	300	200	020	270	50C	1	200	060	017	-43	35	10.9	24.1
T	1000	300	200	020	180	50C	2	330	105	107	2	30	10.9	19.1
T	1000	300	200	080	090	M14	2	800	240	197	-43	35	10.9	24.1
T	1000	300	200	080	000	M14	3	920	280	287	7	10	10.9	9
T	1000	300	200	080	270	M14	2	1240	020	017	-3	30	10.9	19.1
T	1000	300	200	080	180	M14	3	330	105	107	2	30	10.9	19.1
1	1000	300	200	080	090	50C	1	800	240	197	-43	30	10.9	19.1
T	10 10	300	200	080	000	50C	3	920	280	287	7	10	10.9	9
T	1000	300 300	200	080	270 180	50C	2	1240	020	<pre>017 107</pre>	-3 -3	30	10.9	19.1
T	1200	300	50	020	390	M14	1	800	240	194	-46	30	2.4	29·1 27·6
Ť	1200	300	50	020		M14	1	1100	330	284	-46	20	2.4	17.6
Ť	1200	300	50	020	270	M14	1	230	075	014	-51	0	2.4	-2.4
T	1200	300	50	020	180		1	500	150	104	-46	30	2.4	27.6
T	1200	300	50	020	090	50C		800	240	194	-46	30	2.4	27.6
T	1200	300	50	020	600		1	1100	330	284	-46	20	2.4	17.6
T	1200	300	50	020	270	50C	1	220	070	014	-56	10	2.4	7.6
T	1200	300	50	020	180	50C	1	500	150	104	-46	30	2 • 4	27.6
1	1200	300	50	080	090	M14	1	800	240	194	-46	10	2.4	7.6
T	1200	300	50	080		M14	1	1050	325	284	-41	35	2.4	32.6
T	1200	300	50	080	270 180		1	220 340	070	104	-56 -6	20	2.4	17.6
ī	1200			080		M14 50C			240		-46	20	2.4	42.6
1	1200	200	10	000	090	200	1	000	240		-40		2 • 4	11.0

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r	1200	300	50	080	000	50C	1	1100	330	284	-46	30	2.4	27.6	
T	1200	300	50	080	270	50C	1	220	070	014	-56	20	2.4	17.6	
T	1200	300	50	080	180	,50C	1	500	150	104	-46	10	2.4	7.6	
T	1200	300	200	020	090	.M14	3	1230	015	194	179	30	9:5	20.5	4
T	1200	300	200	020	000	M14	2	915	277	284	7,	10	9.5	5	
T		4		020	270	M14	2	1250	025	014	-11	30	9.5	20.5	
T	1200				180	M14	2	340	110	104	-6	30	9.5	20.5	
T	1200	300	200	020	090	50C	1	800	240	194	-46	35	9 . 5.	25.5	
T	1200		and the same			50C	2	920	280	284	4	10	9.5	. 5	
T	1200	300	200	020	270	50C	3	1250	025	014	-11	30	9.5	20.5	
T	1200	300	200	020	180	50C	2	340	110	104	-6	30	9.5	20.5	
T	1200	300	200	080	090	M14	1	800	240	194	-46	30	9.5	20.5	
T	1200	300	200	080	000	M14	1	1030	315	284	-31	45	9.5	35.5	
T	1200	300	200	080	270	M14	2	1230	015	014	-1	30	9.5	20.5	
T	1200	300	200	080	180	M14	2	800	240	104	-136	35	9.5	25.5	
T	1200	300	200	080	090	50C	1	800	240	194	-46	30	9.5	20.5	
T	1200	300	200	080	000	50C	3	900	270	284	14	0	9.5	-9.5	
T	1210	300	200	080	270	50C	2	1245	022	014	-8	35	9.5	25.5	
T	1200	300	200	080	180	50C	1	510	155	104	-51	30	9.5	20.5	

ACCEPTANCE TEST DATA

							H	制	FIA	f	i cili	17.00	SIFICI		
A			50									30	4.9	25.1	
A		0.000												-4.9	
A															
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A	500	300	50												
A	500	300	50												
A	500	300	50	20											
A	500	300	50	80	90	M14	1	800	240	211	29			30.1	
A											-9	30	4.9	25.1	
A								100	030		-1	30		25.1	
A								915	247		34	30		25 1	
1															
A	500	300	50						The second						
A	500	300	50	80	0			400							
A		300	200	20	90	100000	_			211	6			11.	
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A	1000	300	200	80	180	50C	2	345	112	107	5	30	10.9	19.1
A	1200	200	50	20	90	M14	1	800	240	190	50	35	2.4	32.6
A	1200	200	50	20	0	M14	1	1100	330	280	50	25	2.4	22.6
A	1200	200	50	20	270	M14	1	200			50	15	2.4	12.6
A	1200	200	50	20	180	M14	ō	200	000	100	30	10	2.4	12.00
A	1200	200	50	20	90	50C		800	240	190	50	30	2.4	27.6
A	1200	200	50	20	0	50C	1	1115	337	280	57	30	2.4	27.6
A	1200	200	50	20	270	50C	2	1215	007	010	-3	45	2.4	42.6
A	1200	200	50	20	180	50C	1	845	262	100	162	45	2.4	42.6
A	1200	200	50	80	90	M14	1	800	240	190	50	30	2.4	27.6
A	1200	200	50	80	0	M14	2	915	277	280	-3	15	2.4	12.6
A	1200	200	50	80	270	M14	2	1200	000		-10	25	2.4	22.6
A	1200	200	50	80	180	M14	1	500	150	100	50	20	2.4	17.6
A	1200	200	50	80	90	50C	1	800	240	190	50	30	2.4	27.6
A	1200	200	50	80	0	50C	2	915	277	280	-3	15	2.4	12.6
A	1200	200	50	80	270	50C	1	215	067	010	57	30	2.4	27.6
A	1200	200	50	80	180	50C	1	500	150	100	50	20	2.4	17.6
A	1200	200	200	20	90	M14	1	745	232	190	42	40	9.4	30.6
A	1200	200	200	20	0	M14	2	1030	315	280	35	45	9.4	
A	1200	200	200	20	270	M14	2	1230	015	010	5	30	9.4	35.6
A	1200	200	200	20	180	M14	1	445	144	100	44	30	9.4	20.6
A	1200	200	200	20	90	50C	2	800	240	190	50	35	9.4	20.6
1	1200	200	200	20	0	50C	2	915	277	280	-3	15	9.4	25.6
A	1200	200	200	20	270	50C	2	1230	015	010	5	30	9.4	20.6
A	1200	200	200	20	180	50C	2	330	105	100	5	30	9.4	20.6
A	1200	200	200	80	90	M14	1	745	232	190	42	30	9.4	20.6
A	1200	200	200	83	0	M14	4	143	232	280	42	20	9.4	10.6
A	1200	200	200	80	270	M14	2	1230	015	010	5	40	9.4	30.6
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Α	1200	200	200	80	90	50C	1	800	240	190	50	30	9.4	20.6
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В	500	300	50	20	0	M14	1	500	150	301	-151	35	4.9	30.1
В	500	300	50	20	270	M14	2	1000	300	031	91	15	4.9	10.1
В	500	300	50	20	180	M14	2	1100	330	121	151	15	4.9	10.1
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В	500	300	50	80	0	M14	1	1100	330	301	29	40	4.9	35.1
B	500	300	50	80	270	M14	2	100	030	031	-1	35	4.9	30.1
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В	500	300	200	20	0		2	955		301	-4	30	19.0	11.
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В	1200	200	200	20	90	50C	2	800	240	190	50	35	9.4	25.6
В	1200	200	200	20	0	50C		1045	322		42	40	9.4	30.6
В	1200	200	200	20	270	50C		200	060		50	35	9.4	25.6
B	1200	200	200	20 80	180	50C		315	097		-3	40	9.4	30.6
В	1200	200	200	80	0	M14	2	815 1045	247 322		57 42	30 45	9.4	20.6
В	1200	200	200	80	270	M14	2	200	060		50	30	9.4	35.6
В	1200	200	200	80	180	M14	1	445	142		42	20	9.4	10.6
В	1200	200	200	80	90	50C	1	815	247	190	57	30	9.4	20.6
В	1200	200	200	80	0	50C	4	915	277	280	-3	20	9.4	10.6
f	1200	200	200	80	270	50C	2	200	060		50	45	9.4	35.6
b	1200 500	200	200	80	180	50C	1	445	142		42	20	9.4	10.6
C	500	300	50 50	20	90	M14	0	045	202	211	0	16	4.9	
C	500	300	50	20	270	M14 M14	2	945	292 030		-9 -1	15 30	4.9	10.1
C	500	300	50	20	180	M14	1	515	157	121	36	45	4.9	25 • 1 40 • 1
C	500	300	50	20	90	50C	2	730	225		14	30	4.9	25.1
C	500	300	50	20	0	50C	2	945	292		-9	0	4.9	-4.9
C	500	300	50	20	270	50C	2	105	032	031	1	30	4.9	25.1
C	500	300	50	20	180	50C	1	415	127	121	6	40	4.9	35.1
C	500	300	50	80	90	M14	2	600	180	211	-31	50	4.9	45.1
C	500	300	50	80	270	M14 M14	2	945	292	301	-9	20	4.9	15.1
C	500	300	50	80	180	M14	0	100	030	031	-1	40	4.9	35.1
C	500	300	50	80	90	50C	1	800	240	211	9	30	4.9	25.1
C	500	300	50	80	0	50C	2	945	292	301	-9	25	4.9	20.1
C	500	300	50	80	270	50C	2	1100	330	031	-61	90	4.9	85.1
C	500	300	50	80	180	50C	0			121			4.9	•
C	500	300	200	20	90	M14	2	300	090	211	-121	35	19.0	16.
C	500 500	300	200	20	0	M14	3	945	292	301	-9	30	19.0	11.
C	500	300	200	20	270 180	M14 M14	3	100	030	031	-1	30	19.0 19.0	11.
C	500	300	200	20	90	50C	2	645	202	211	-9	30	19.0	11.
C	500	300	200	20	0	50C	2	945	292	301	-9	30	19.0	11.
C	500	300	200	20	270	50C	2	130	045	031	14	40	19.0	21.
C	500	300	200	20	180	50C	2	430	135	121	14	40	19.0	21.
C	500	300	200	80	90	M14	1	800	240	211	29	30	19.0	11.
C	500	300	200	80	0	M14	2	930	285	301	-16	30	19.0	11.
C	500	300	200	80	270 180	M14	3 2	105	032	121	-1	30	19.0	26.
C	500	300	200	80	90	50C	2	645	202	211	-9	20	19.0	11.
C	500	300	200	80	0	50C	2	920	280	301	-21	30	19.0	11.
C	500	300	200	80	270		2	1250	025	031	-6	40	19.0	21.
C	500	300	200	80	180	50C	2	415	127	121	6	30	19.0	11.
C	1000	300 300	50	20	90	M14	0	10/5	200	197			2.7	
C	1000	300	50	20	270	M14	1	200	322	287 017	35 43	30	2.7	27.3
C	1000	300	50	20	180	M14	0	200	000	107	43	30	2.7	27.3
C	1000	300	50	20	90	50C	1	815	247	197	50	30	2.7	27.3
(1000	300	50	20	0	50C	2	915	277	287	-10	0	2.7	-2.7
(1000	300	50	20	270		2	1230	015	017	-2	30	2.7	27.3
C	1000	300	50	20	180		0			107			2.7	•
C	1000	300	50	80	90	M14	1	800		197	43	30	2.7	27.3
C	1000	300	50	80	270	M14	1	1100	062	287	43	40	2.7	37.3
C	1000	300	50	80	180	M14	0	200	002	107	47	50	2.7	27.3
C	1000	300	50	80	90	50C	0			197			2.7	•
C	1000	300	50	80	0	50C	1	1050	325	287	38	40	2.7	37.3
C	1000	300	50	80	270	50C	2	1215	007		-10	40	2.7	37.3
C	1000	300	50	80	180	50C				107	PRESE	7 71	27	
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		C	1000			20	90	M14	1		255	197	58	30	10.9	
		C	1000		200	20	270	M14	3	900	270 055	287	-17	50	10.9	39.1
		C	1000		200	20	180	M14	2	500		107	38	25	10.9	19.1
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		C	1000		200	20	0	50C		940	290	287	3		10.9	19.1
		C	1000		200	20	270	50C			050		33	30	10.9	19.1
***		C	1000			80	180	50C	1	530	165	107	52	30	10.9	19.1
		C	1000		200	80	0	M14	0	130	045	197	-118	45	10.9	34.1
		C	1000		200	80	270	M14	2.7	1215			-10	45	10.9	34.1
	4 4	C	1000		200	80	180	M14			150		43	20	10.9	9.1
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		0	1000	- Sec. 1995	200	80	270	50C	2	915 1210		287	-10 -12	20 45	10.9	9.1
to the		C	1000		200	80	180	50C			150		43	30	10.9	34.1 19.1
	- 30	C	1200		50	20	90	M14	1	745	232	190	42	30	2.4	27.6
		C	1200		50	20	0	M14	1	1100			50	30	2.4	27.6
		C	1200		50 50	20	270 180	M14		145	052		42	30	2.4	27.6
		c	1200		50	20	90	50C	1	830	255	100	65	75	2.4	72.6
		C	1200	200	50	20	0	50C	1	1100			50	30	2.4	27.6
		(1200		50	20	270	50C	1	145	052	010	42	30	2.4	27.6
		7	1200 1200		50	20 80	180	50C M14		800	240	100	F 0	20	2.4	27.
		c	1200	200	50	80	0	M14	1	1045	240 322	280	50 52	30 35	2.4	27.6 32.6
. 9		C	1200		50	80	270	M14	-	150		010	40	30	2.4	27.6
		C	1200		50	80	180	M14				100			2.4	•
		C	1200	200	50 50	80	90	50C		815	247		57	30	2.4	27.6
4 4 3		C	1200	200	50	80	270	50C		905 210	272 065		-8 55	20 35	2.4	17.6 32.6
		C	1200	200	50	80	180	50C		450	145		45	20	2.4	17.6
200		C	1200	200	200	20	90		1	750	235	190	45	35	9.4	25.6
*		C	1200	200	200	20	0	M14		345		280	-168	30	9.4	20.6
		C	1200	200	200	20	270 180	M14 M14		200	060	100	50	30	9.4	20.6
		C	1200	200	200	20	90	50C		630	195		5	30	9.4	20.6
		C	1200	200	200	20	0		2	1100	330	280	50	45	9.4	35.6
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APPENDIX B

This appendix is a copy of the test plan as submitted to the Limited War Laboratory on 2 July 1968.

Test Plan: Improved Acoustic Locator System (Final Draft) 2 July 1968

- I. Introduction
- II. Test Equipment
- III. Range Layout
- IV. Test Schedule
- V. Test Procedures

Appendix A: Test Plan Rationale

Appendix B: Data Analysis

I. INTRODUCTION

This test program has been designed for conduct in certain numbers of tests called "blocks". One block of tests includes 180 separate tests using all weapons at one range location. These weapons fire at the aircraft from four aspects. The aircraft will fly at 5 different altitudes and 3 different speeds. A full block of tests will require approximately 3% hours of work. In order to conduct tests of special conditions, portions of these test blocks will be run to obtain results of detection and location accuracy.

With this design of test blocks and portions of blocks for special tests, a good program can be expected even with unforseen circumstances presenting themselves. The total program can be reduced, changed or expanded to meet all circumstances.

This copy of the test plan supersedes the initial draft submitted to the LWL on 25 June 1968.

II. TEST EQUIPMENT

The equipment for these tests will consist primarily of existing, common and readily available items of equipment. For this discussion the equipment needed is divided into three groups as noted below.

(1) Range layout equipment

2 surveyor's transits

2-100 ft steel tapes

500 ft of engineers tape

25 wooden pegs

The range layout will consist of measuring off and marking the 18 firing points, the two a/c locator sites, and the range marker as noted in figure one. The points having been located by use of the tape and the transits, they would be marked for later use by driving the wooden stakes into the ground at each location. It would be desirable that the stakes each have written on them the point which it represents. The range marker will be located by laying white engineers tape in a cross of 100 ft legs in the direction of the 4 points of the compass N-E-S-W.

(2) Basic testing equipment (for the field)

- 1 UH-1B helicopter
- 1 UH-1D helicopter
- ? Improved Acoustic Locator Systems
- 1 22 caliber set of weapons
- 1 30 caliber set of weapons
- 1 50 caliber set of weapons
- 2 aircraft locator items of equipment
- $1\frac{3}{4}$ ton truck with radio (type?)
- 3 hand held radios
- l field table
- 2 folding chairs
- 1500 rounds of 22 caliber ammo
- 1500 rounds of 30 caliber ammo
- 1500 rounds of 50 caliber ammo
- ? compass(s)
- 1 wind measuring device

The weapons, ammo, ILAS, and helicopters requirements are basic to the test and no further discussion of them will be presented here. The items to be used to locate the helicopter during the tests are dependent upon the accuracy desired of test results. Their purpose is to aid the observer in locating the a/c at the precise time the weapon is fired. This is to allow for development of valid azimuth and depression angle information against which the test data can be compared in order to reveal the accuracy of location of the weapon from the system being tested. The $\frac{3}{2}$ ton truck is needed for transportation of personnel and equipment to and from the range

each day. The radio in the truck and the 3 walkie talkie type radio uses are discussed in Section IV of this plan. The field table and chairs are needed to provide a reasonable condition for the recording of data in the field. The wind measuring device is needed for recording the wind speed and direction during the tests. Some type of compass is needed to aid in "surveying" the guns each day to assure they are aimed in a direction parallel and perpendicular to the a/c line of flight.

(3) Personnel

- 1 Test Director
- 1 Pilot
- 1 Co-pilot
- 3 Weapon Crew
- 1 Data Recorder
- 2 a/c Position Locators

Variations of this test crew as well as the duties of each are discussed in Section IV. In addition to these persons for test conduct, approximately 3 persons will be needed prior to the tests for the layout of the range.

III. RANGE LAYOUT

The real estate over which these tests can be conducted will require approximately 30-40 acres with a geometric pattern of approximately 1 = 2w. It would be desirable that the land be slightly wooded, but not so as to prevent the observation or restrict the flight path of the flying helicopters at the ranges and altitudes noted in this plan. Although the vegetation, topography, bodies of water, etc., will influence the operation of the system, it is not a factor in the factorial design of these tests. The condition of the terrain will be documented and results of the system under other conditions of terrain can only be estimated. In order to facilitate range layout and accuracy figures, it is desirable that the land be relatively flat. The layout of the range should ultimately be as shown in Figure 1. This shows basically one range marker over which the a/c will be when fired at, two marked sites where persons are positioned to help locate the a/c at the time of firing, and 18 firing points which gives all combinations of miss distance and range believed to be required for evaluation of the system.

Although 30-40 acres should allow for the space needed to establish the points required on the range, the use of live ammunition will obviously require the use of a downrange impact area. Since the weapons will all be fired in the same direction and the firing points will change only daily, during normal testing the size of a very small firing fan can be determined each day. This fan would be defined by the range of weapon being used on a given day and by the maximum deflection error of the weapon at its maximum range.

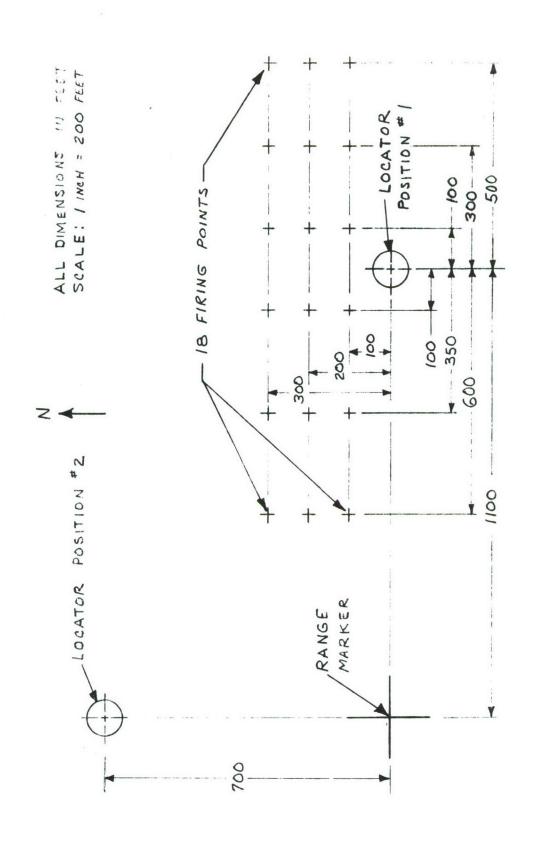


FIG. 1; RANGE LAYOUT

It is envisioned that the range layout will consist of merely marking a ground position for the locator points and for the firing points. The range marker should consist of white engineer tape positioned in the manner shown with the length of each of the four legs being 100 ft. These legs indicate the desired flight path during the tests. In the event that night testing is desired or required, the range marker would consist of battery powered lights—9 of one color in one line and 9 of another color in the other line.

IV. TEST SCHEDULE

The design of these tests is such that distinct breaks are realized at the conclusion of 4 tests, 12 tests, 36 tests, 180 tests, 540 tests and 3240 tests. These breaks are when there is a change in one of the controlled factors of the test. This is more fully discussed in Section IV, but the proposed program will be conducted in 18 blocks of tests each requiring an estimated 3-3/4 hr of the aircraft flying over the range. In addition to these 18 blocks of tests, various demonstrations as discussed later will be required during the test program. It is envisioned that a particular test day will allow for the completion of one block of tests plus about 1-2 hr for additional work if needed. Therefore, the approach has been to develop a priority listing of the blocks of tests (see Figure 2), assign them a particular test day and expect to conduct the particular demonstrations on off days or at the day's end of a particular block of tests. As is indicated in Section IV, one block of tests consists of the total activity required at one of the eighteen firing points.

Miss			R	ange		
Distance	500	750	1000	1200	1400	1600
300	J	M	В	R	E	I
200	D	G	N	L	Q	С
100	P	A	H	F	K	0

FIGURE 2. PRIORITY OF TEST BLOCKS

If a maximum of one block of tests are conducted each test day, the tests could be completed from 8 June through 31 June. Allowing for some unforseen circumstances such as range scheduling, a/c maintenance, weather, etc., the testing rate would be slowed but not excessively unless the program cannot be completed by August 16. The establishment of the priority of test blocks should allow minimum analysis problems if the test program is cancelled at any time. With this assumption, the program would terminate no earlier than June 31 with all tests completed or not later than August 16 with any portion or all of the tests completed.

To complete 1 block of tests, the aircraft would fly the prescribed course a minimum of 45 times, be fired at 180 times at combinations of three speeds and five altitudes. Each of the three sets of weapons will fire 60 times during the block of tests.

The actual tests should begin on 8 June with the previous week set aside for range layout, equipment installation and check-out and for pilot testing. Pilot testing should provide for final definition of communication procedures, firing procedures and data recording procedures.

It is felt that the weapon performance and the IALS performance will dictate the maximum range and miss distance which should be investigated during these tests. These have been defined as 1600 ft range and 300 ft miss distance. If initial testing would reveal information which indicates these two factors are not the reasonable maximums, the plan should be altered to obtain additional information at perhaps 1800 ft range and/or 400 ft miss distance. These changes cannot be anticipated at this time, but the test design change would merely call for assigning a priority to each of the additional factors and "fitting" them into the proposed sequence of tests. Time and resources would then again dictate the termination of the testing.

The design of the major portion of the program is such that each day's activity can be defined as a block or blocks of tests. Because of this, blocks of tests can easily be added, deleted, or changed without disrupting the overall test schedule.

V. TEST PROCEDURES

For these tests the locator site #1 (LS-1) will be the position where three persons will be operating. They are the locator man, the data recorder, and the Test Director (TD). Three-way communications would be established between the firing point (FP) and each of the locator sites. Two-way communication is needed between the aircraft and the locator site #1. The TD should be able to continually inform the pilot of the speed and altitude he is to maintain over the range marker. This information is presented in Figure 3. The co-pilot reading the scope in the aircraft must be able to transmit his interpretation of the system performance to the data recorder. The locator points should be in communication with the firing point in order to give the order for "fire" at the proper time. Communication during the tests would be somewhat like as follows:

TD to pilot - "Pass west at 200 ft and 40 knots"

LS-2 to FP - At the time the aircraft is over the firing point - "Fire"

Copilot to - "Audio, 3 points, azimuth 160°, deflection 20°" LS-1

Figure 3; A/C PROCEDURE FOR EACH BLOCK OF TESTS

1 15 0 24 20 40 3 0 26 80 4 40 27 200 80 5 40 27 200 80 6 40 28 500 0 7 80 32 40 0 10 50 0 33 40 0 11 0 34 80 40 12 80 34 80 13 40 33 40 0 14 40 34 80 40 16 80 40 40 40 17 80 40 40 18 50 80 40 40 20 80 40 40 40 10 6 42 40 40 21 0 42 40 40 22 40 42 40 40 23 40 44 40 40 24 40 40 40 40 25 40 42 40 40 26 40 42 40 <td< th=""><th>Run Number</th><th>Altitude</th><th>Speed</th><th>Run Number</th><th>Altitude</th><th>Speed</th></td<>	Run Number	Altitude	Speed	Run Number	Altitude	Speed
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40 35 500 8 40 37 1000 8 80 39 40 80 40 40 50 80 41 42 200 0 43 8 0 44 8 8 40 8 8 40 8 8 40 8 8 40 8 8 40 8 8 40 8 8 40 8 8	11		0	34		80
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40 37 1000 80 39 80 40 50 80 41 200 0 42 0 43 8 40 44 8 40 44 8 40 8 8 40 8 8	13		40	36	200	80
50 80 200 0 40 41 42 42 6 43 6 44 40 44 40 88 8 44 40 88 40 88 40 88 40 88	14		40	37	1000	0
80 39 80 40 200 0 42 42 0 43 0 44 40 45 40 8	15		40	38		0
50 80 40 200 0 42 0 43 0 44 40 45 1000	16		80	39		0
50 80 41 200 0 42 0 43 0 44 40 45 1000	17		80	40		40
200 0 42 0 43 0 44 40 45 1000	18	50	80	41		40
0 43 0 44 40 45 1000	19	200	0	42		40
1 0 44 2 40 45 1000 3 40	20		0	43	-	80
2 40 40 3	21		0	44		80
3	22		40	45	1000	80
	23		40.			

		* *
TD to Pilot	-	After assuring that data are recorded -
		"Pass north" - Pilot does a 270° turn back
		over the range marker without changing speed
		or altitude
LS-1 to FP	-	At the time the aircraft is over firing point -
		"Fire"
Copilot to	-	"Audio, 3 points, azimuth 90°, deflection 20°"
LS-1		
TD to pilot	-	"Pass east"
LS-2 to FP	-	"Fire"
Copilot to	-	"Audio, 3 points, azimuth, deflection
LS-1		
TD to pilot	-	"Pass south"
Copilot to	-	"Audio, 3 points, azimuth, deflection"
LS-1		
TD to FP	-	"Ready with Weapon 2"
FP to TD	-	"Weapon 2 ready"
TD to pilot	-	"Pass west at 200 ft and 40 knots"
etc.		

Safety precautions are most critical during the pass to the north. (See Figure 4.) At this time the bullet is being fired in front of the a/c and any delay in firing could be noticed. During this pass the miss distance should be primarily in the vertical direction. This is to be accomplished by the a/c maintaining 15 ft additional altitude than on other passes during the same run.

Any of the special tests, i.e., loaded helicopter, UH-1D instead of UH-1B, etc., would be run in a similar manner. Weapon sequence and elevation angles to be set when firing for each run at a particular range is as noted in Figure 5. Samples of the two basic data forms appear on pp. 15 and 16.

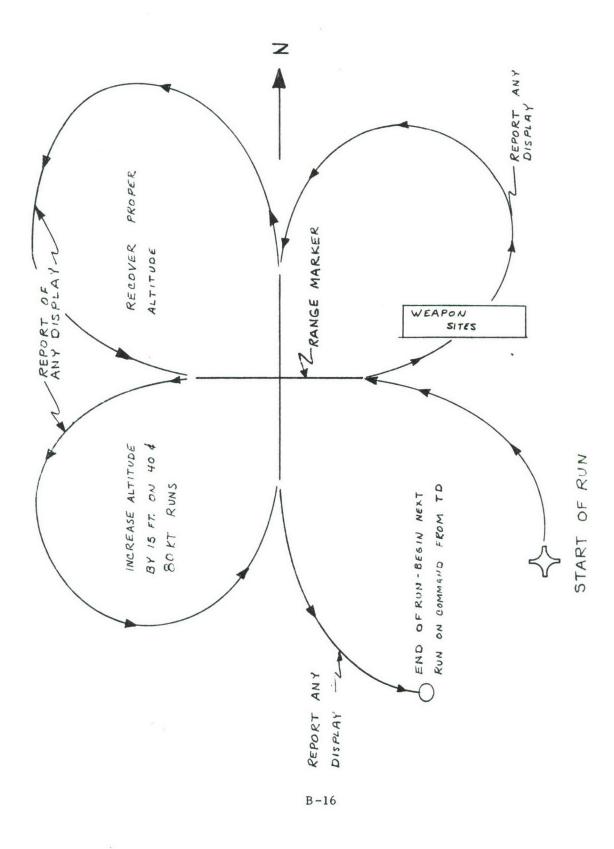


FIGURE 4; CLOVERLEAF FLIGHT PATTEEN

Run	Weapon	¥7.	El	evation A	Angle at	Range	
Number	Caliber	500	750	1000	1200	1400	1600
,	 		1				
1	22	1.7	1.3	1.0	.8	.7	.5
2	30	1 1			1	1	1
3	50	1					
4	22						
5	30		1 1				
6	50						
7	22						
8	30	1		- 1		1	
9 .	50	1.7	1.3	1.0	.8	.7	.5
10	22	5.7	3.9	3.0	2.3	2.1	1.9
11	30	11	1	1	1	1	
12	50					1 1	
13	22						
14	30						
15	50 ·						
16	22						
17	30			1	1		
18	50	5.7	3.9	3.0	2.3	2.1	1.9
19	22	21.8	15.0	11.3	9.5	8.2	7.1
20	30				1	1	1
21	50						
22	22						
23	30						
24	50	1.					
25	22						
26	30				1		1
27	50	21.8	15.0	11.3	9.5	8.2	7.1
28	22	45.0	34., 0	26.7	22.6	19.7	17.3
29	30	11		1	1	1	1
30	50	_					
31	22.						
32	30 .						
33	50	4					
, 34	22						
35	30		1	1.	1		1
36	50		34.0	26.7	22.6	19.7	17.3
. 37	22	63.5	53.3	45.0	40.0	35.8	32.0
38	30	11	. 1		1		
39	50						
40	22						
41	30						
42	50						
43	22						
44	30 50				l		1
45		63.5	53.3	45.0	40.0	35.8	32.0

Figure 5; ELEVATION ANGLES

RANGE 750

MISS DISTANCE 100

DATE:		MISS DISTANCE	4.60
WEATHER: _			× .
WEATHER			ander in representation can retire outling to Lacutor / Angelor to constitute and a section of contract decrees
WINO:	SPEED	DIRECTION	
0800		• •	
1000		Will be State of State and	
1200	Bullion, the dissertation or servings.		
1400		Note that the same particular and	- W
1600			
COMMENTS:			
TEST DIREC	TOR:		
PILO	r :		
	-		
GUN CRE W			
			THE PARTY OF THE P

RUN NO.	FIRE FROM	ROUNDS	AUDIO	NO. OF DOTS ON SCOPE	AZ IMUTH	:DEPRESSION ANGLE	FALSE ALARM	1	REMA	RKS
1	A R F L	,			,					
2	A R F					¥			,	
3	A R F L							t .	90	
4	ARFL			·		¥				•
5	A R F L									
6	A R F L									
7	A R F L		8							
8	A R F L								H 1.	,
9	A) R F									

The data recorder positioned at LS-1, where he is able to monitor both radio nets, will be recording the data from these tests. He will have one page of the form on which will be recorded the data from the 36 tests at one altitude. This will then require 5 pages of data from a block of tests on each day plus any data from special test runs on that day. Since condition of altitude, range, weapon, etc., are to change more frequently for special tests, data recording is less voluminous but more critical. In addition to the data forms already mentioned, it is desirable that another form be completed daily which will privide any opinion and comments from the seven participating personnel. First entry should be by the data recorder where he should note the daily weather conditions including wind direction and velocity, temperature and humidity. At the day's completion, comments should be solicited from the a/c crew, the locator men, the gun crew and especially the test director. These forms are provided in packages with this plan and are noted for each activity. When the sequence to testing varies from the planned, the package must be revised to insure the correct forms are made available to the data recorder. At day's end or periodically, the completed forms should be reproduced and one copy provided to ORI so that data reduction and analysis can begin as soon as possible.

Some of the special tests to be run during the program are as noted below:

Use the UH-1D instead of the UH-1B

Fire multiple shots instead of single rounds

Increase the gross weight of the UH-1B

Firing of special weapons

Firing from multiple positions

Testing of the additional IALS

Flying at 100 knots

Table 1 reveals the particular runs to be made during 5 of these special tests. Separate data collection packages are provided for each test.

TABLE 1 SPECIAL TEST ACTIVITY

Estimated Completion Time	1 hr	1 hr	1 hr	1-1/2 hr	1 hr
Runs	10-18 of block G 28-36 of block R	19–27 of block N 37–45 of block A	10-36	10-15 and 28-33 of blocks J, H, & Q	1, 2, 3, 19, 20, 21 of blocks R & M
Special Condition	Replace the three basic weapons to be used during the tests with the $M-1$, 30 cal Mg and the $37~\mathrm{mm}_{\bullet}$	Replace the three basic weapons with the M-1, 12.5 mm and the AK.	Use the M-1, 12.5 mm and the AK at Block A firing point. Use the 3 basic weapons at Block R firing point. Fire simultaneously - one weapon from each point.	Fire multiple rounds from each weapon.	Make all runs at 100 knots a/c speed.
Number	г	2	ო	4	Ŋ

Due to the amount of equipment to be transported to the range daily, it is required that the range crew have a 3/4-ton truck for their use on test days. In the truck can be mounted the radio set to be used for contact between the Test Director and the aircraft crew. Radios for contact between the firing points and the locator points should be a different net and this communication might be accomplished by means of a "walkie talkie" type set. Dependent upon the type of locating device available, the transit man might need a headset type arrangement in order to free his hands for operation of the device.

To be transported to the range daily in the truck would be the following:

7 people - TD, 2 location men, 1 data recorder, 3-man weapon crew

3 weapons (minimum)

180 rounds of ammo (minimum)

l field table

2 folding chairs

3 radios - for locator sites and firing point

Lunch?

Data forms for the tests to be run on that day

Equipment for any of the special tests on that day.

One of the seven men might be eliminated by allowing the operation at locator point #1 to be performed by two men instead of three. This could free the test director so that he can move freely between the locator points, the firing points and to ride in the aircraft. The "best" procedure for this should be determined during the pilot tests.

Another alternative for the reduction of personnel would be to eliminate locator point #2 and move locator point #1 to a position SE of the range marker and from here locate the a/c in both the N-S and E-W paths.

Without the use of any locator points, two alternatives are available.

- (1) Position a man at the range marker intersection who would locate the a/c merely by sighting him directly overhead and giving the "fire" command, or
- (2) Allow the pilot to locate himself over the range marker and calling for fire himself.

If location accuracy of the system is of significance, the first alternative is bad, and if any degree of gaming is desired, alternative 2 is bad. Resources and desired accuracy of the results should dictate which alternative must be used.

APPENDIX A TEST PLAN RATIONALE

The purpose of this test program is to evaluate the performance of the Improved Acoustic Locator System (IALS) during live firing conditions in order to determine its operational capabilities and limitations.

The IALS was developed in response to a small development requirement (SDR) for a bullet detection device for Army aircraft. Paragraph 2a of the SDR states the purpose of the development as follows:

"A device to detect and indicate to aircrews of tactical aircraft the near passage of projectiles, and to indicate the direction from which fire originated in both horizontal and vertical angles from the aircraft."

The operational characteristics of the device are specified in paragraph 2b of the SDR.

Department of the Army Approved Small Development Requirement for a Bullet Detection Device for Army Aircraft (U), 22 October 1965, CONFIDENTIAL.

The test plan described in this report was designed to gather data for use in describing the system performance in terms of (a) probability of detection of ground fire and (b) accuracy of location of the source of the fire as functions of the factors that affect these two parameters. Reference material 2.3 was reviewed and discussions were held with personnel at LWL to identify the factors, and their levels, to be considered in the test design. Table A-1 lists the factors incorporated into the test design and the levels of each factor along with a brief statement of the affect of each factor on system performance and the applicable operating characteristics, if any, specified in the SDR.

Additional factors that do influence the system performance and that are not listed in Table A-1 include the type of terrain over which the aircraft is operating and the depression angle of the source of fire relative to the aircraft. The probability of detection of the reflected ballistic shock (RN) wave and the muzzle blast varies considerably from a wooded to a non-wooded area. This factor was not considered because of the inconvenience of using different test sites. The accuracy of location varies with depression angle. Although not specifically listed in the table, this factor is considered with the different ranges and aircraft altitudes included in the test design.

Six of the factors listed in Table A-1 were included in the factorial design of a set of tests intended to gather data for statistical analysis to describe the probability of detection of ground fire and accuracy of location of its source. To conserve test time, three additional factors are considered in individual tests intended not to gather data for statistical analysis but to describe system performance under these conditions.

^{2/} J. Wenig and H. Forst, <u>An Airborne Acoustic Locator System</u> (U), U.S. Army Limited War Laboratory Draft Report, CONFIDENTIAL.

^{3/} U.S. Army Limited War Laboratory, Acoustic Locator System (U), Technical Report LWL-CR-08P3, September 1967, CONFIDENTIAL.

Foctors Affecting Penformance of the Improved Acoustic Location System. Table A-1.

1		-			
Tree Took	1	. Factorial Test	Design	Single Demon- strations	
Levels	1400/1600s	00 100 H	14 and 2.5 mm, 37.	de l	
Suggested Levels for Test	Slont range to 1000ft (E) Horizontal ranges of 3000 ft (D). 500,750,1000,1200, 1400,1606ft To 100m (E); 300m (b) 100,200,300 ft,	Slant range, as above, 15,50,200,500,100 H, only system not to be ad- 0,40,80 km.	Device to detect pro- M-16, M-1, M-14 and Device les as small as, 22 .30 cal; AK, 12,5 mm, 37 mm.	enemy ground fire, enemy ground fire, unloaded, typical unloaded, typical unloaded, typical unloaded, typical unloaded, typical second.	
S S	(c) How	75, 0,	300	Malo WH	
Operational Characteristic From SDE; Essential(E) and/or Desiroble (D)	1000ft (1	Start range, as above only. System not to be ad- versely affected by	Orvice to detect pro-	posed Fine,	
1 Char ; Esse	(E):3	C, as t to b ffecte	small small	A/C ex bund to 17	
nationa n SDP afor D	3000 FL (0).	Slant range, as above only system not to be adversely affected by socool of AC	les as	Rie Army A/C exposed enemy ground fire, Rates up to 17 per second.	
900	7 5		Dear Leed Leed Leed Leed Leed Leed Leed Lee	11 1 1	CON HISTORIA MINISTERIO A NEW PROPERTICIONA NA CALLO
1) (, !!	Affects probability of detection of RN-wave and MB, hence Slont range to 1000ft (E) Horizontal ranges of ability to locate. ASOD F. (D). Affects probability of detection of N-wave. To 100m (E); 300m (b) 100, 200, 300 ft,	Ambient noise is a function of AIC altitude, hence, of the delection of signals. Ambient noise is a function of AIC speed, affecting knobability of detection of signals, AISO, AIC speed of focation.	07	Ambient noise is a function of Alc type, affecting imbient noise varies with Alc load, affecting Po. Ability of operator to interpret displays hence, Al. is a function of rate of five.	
retor	liss histonice	Speed	Osapon Zimeth Zimeth Seletive to Finaraft)	Type Type Incraft Load -ate. of	B-26

The schedule and manner of conduct of the factorial tests described in Sections III and IV provide for the collection of large quantities of data in relatively short time periods. The ability of the observer to collect meaningful, accurate data is considered to be the limiting criterion for determining the number of individual tests to be conducted in a unit of time.

The range layout and test procedures group the tests into blocks of 180 data points. Each block of tests can be conducted in an estimated 3 3/4-hr time period. This time period is based on an estimate of 5 minutes for the aircraft to run a pattern of 4 flights, at different azimuths, over a reference point. This 5-minute period is believed to provide sufficient time for the observers to collect data. Each block of tests can be conducted with the gun crews at a single position, varying their weapons, and with the aircraft operating at different aspects, speeds, and altitudes. Range and miss distance are varied from block to block by relocating the gun crew.

Seven different weapons are used during these tests; three weapons are to be used in the factorial tests. The M-16 represents .22 cal.; the M-14 represents the .30 cal.; and the .50 cal. MG represents the third weapon. Special tests are designed to demonstrate the M-1, .30 cal. MG, the AK, the 12.5 mm, and the 37 mm weapon.

Data will be collected on data sheets during the tests for immediate analysis to determine probability of detection and accuracy of location. The signals recorded on magnetic tape are considered to be of use in later detailed analyses.

APPENDIX B DATA ANALYSIS

Data will be available following the tests from two basic sources:

- a. Completed data sheets, with manual entries, will be available for analysis immediately after the testing on a day-by-day basis.
- b. Magnetic tape recordings of selected signals from the IALS and audio comments will be made during the tests by the manufacturer. Information from these tape recordings will available for analysis after some delay for data processing.

The data described in the first paragraph above will form the basis for the analysis to be conducted during this work assignment. These data will be supplemented by information from the magnetic tape and film strip recordings, if available, as necessary and primarily for purposes of clarification.

FACTORIAL TESTS

Data resulting from the factorial tests will be used to describe two measures of the system performance:

- 1. Probability of detection of ground fire, and
- 2. Accuracy of location of the source of fire,

each in terms of the factors that affect the particular measure. These are seemingly simple measures of performance but are complicated by the different ways in which a detection or a location can be made.

The IALS processes and displays all acoustic waves detected by the three microphones in the receiver array. There are three distince signals associated with a given firing and normally detected by the receiver array. In chronological order, they are the bullet shock wave (N-wave) from the bullet as it passes the aircraft, the reflection (RN-wave) of the bullet shock wave from a point on the ground between the weapon and the aircraft, and the wave from the muzzle blast (MB). If all three signals associated with a firing are detected and displayed by the IALS, the operator can easily distinguish among them. The factor that influences the detection of the N-wave most is probably the miss distance. Range and terrain probably influence most the detection of the RN-wave and the muzzle blast. The test design intentionally creates conditions under which the detection of all three signals are likely and under which the detection of the N-wave alone is likely and the detection of the RN-wave and muzzle blast only are likely.

The SDR describes the device to be developed as one to detect ground fire directed at the aircraft. If one signal is received and displayed by the IALS, the operator cannot identify it in terms of N-wave, RN-wave, or muzzle blast. The system does not necessarily distinguish between the following two cases:

- a. Ground fire directed at the aircraft from a long range and resulting in a near miss.
- Ground fire not directed at the aircraft and occurring at a near range.

For purposes of describing <u>system</u> performance during the data analyses, the sounding of an audio alert, which is concurrent with a display on the CRT, will be interpreted as a detection. During later more detailed analyses, using data from the magnetic tape recordings, the probability of detection of each of the three individual signals can be determined as functions of the different factors influencing system performance.

The MB signal provides the most accurate location information. The RN-wave provides fairly accurate location information. The N-wave indicates no information on location of the source of fire but nevertheless is displayed on the CRT. If after a given firing all three signals are displayed, the operator will read azimuth and depression angles from the MB signal. If two signals are displayed, the second will be interpreted for azimuth and depression angles and, at worst, the RN-wave will be used for location. If only one signal is displayed, the angles will be read from the display for describing location. If the one signal happens to be the N-wave, location accuracy will be quite poor. However, for purposes of describing system performance during the data analyses, the interpretation of the last signal to be received and displayed for location information seems to be most reasonable. During later more detailed analyses, using data from the magnetic tape recordings, the accuracy of location can be determined for the MB signal and the RN-wave individually.

As indicated earlier in this discussion, the data to be analyzed during this work assignment will consist most likely of only that recorded on the data sheets during the actual conduct of the tests. One of the six

factors, probably range, will be considered as the dominant factor. Probability of detection and location accuracy will be graphically portrayed as a function of range.

- a. Probability of detection (P_D) will be described as the ratio of the number of audio alerts (or displays) to the number of firings.
- b. Accuracy of location (A_L) will be described in terms of each of the angles, considering both biases and the magnitudes of the errors.

The curves of $P_{\rm D}$ and $A_{\rm L}$ versus range will be plotted, along with appropriate confidence intervals, on what will be considered base charts. For each of the remaining 5 parameters, a family of curves of $P_{\rm D}$ versus range and $A_{\rm L}$ versus range will be plotted on a transparency that can be overlaid on the base chart to enable a quick graphical analysis of the levels of each additional factor that cause significant differences from the basic values. More detailed factorial analyses will then be conducted as individual cases, as appear necessary.

DEMONSTRATIONS

The special tests for assessing the influence of aircraft type, aircraft load, and rate of fire on system performance will be analyzed on an individual basis for the levels of range and miss distance selected. Under these conditions, $P_{\rm D}$ and $A_{\rm L}$ will be compared with the values from the factorial tests to determine significant differences.

APPENDIX C

This appendix is a copy of the work assignment which originated the contractor effort in the testing and analysis of the ALS.

WORK ASSIGNMENT

TITLE: Evaluation of an Acoustic Locator System, Task 08-P-63

1. Work Assignment Number:

6

2. Contract Number:

DAAD05-68-C-0119

3. Background:

The U. S. Army Limited War Laboratory has developed a device, known as the Acoustic Locator System, for use aboard Army aircraft to detect ground fire directed at the aircraft and to locate the source of the fire. The system measures the transit time of an acoustic wave across a three-microphone array mounted on the exterior of the aircraft, alerts the aircrew to the ground fire, processes the signals from the microphone to obtain azimuth and depression angles of the source relative to the aircraft, and displays the location information on a cathode ray tube inside the aircraft

Six Acoustic Locator Systems were tested under live firing conditions at Aberdeen Proving Ground during January 1967. These same systems were then sent to Vietnam for evaluation under combat conditions. Tests and combat usage have proven the acoustic detection and location concept to be sound. Problem areas were identified and an Improved Acoustic Locator System (IALS) has been designed. Improved systems are presently being fabricated and will be available for testing at Aberdeen Proving Ground during the period 1 July to 15 August 1968.

4. Objective:

To develop a test plan by which the IALS can be evaluated, to indicate a method for data analysis and to reduce and analyze the data.

5. Services to be Performed:

The contractor shall study the principle and operating characteristics of the IALS, identify the factors that influence its performance, and devise a test plan for evaluation of the system aboard the UH-1B and UH-1D aircraft during live firings and reduce and analyze the data. The tests will be designed primarily to evaluate the detection capability and location accuracy of the IALS under different operating conditions. The optimization of the read-out devices and the false alarm rates and causes will be secondary considerations.

The test plan will be designed for two levels of testing. The first level will be the detailed testing of at least one system to determine the capabilities and limitations of the IALS aboard each of the two types of aircraft. The second level will be an acceptance test for verifying the operation of each additional system.

Within the constraints of available facilities, time, and money, the test plan will be designed to allow the collection of as much data as possible for evaluation of the system. The constraints are:

- a. Facilities: Those available to the Limited War Laboratory at Aberdeen Proving Ground.
- b. Time: System will be available for testing during the period 1 July to 15 August 1968, however, due to problems in aircraft and range scheduling and inclement weather, the tests should be designed for conduct within a three-week period.
- c. Costs: Total costs of the tests should not exceed \$20,000.

During the tests, data will be collected in the form of manual entries in logs from visual readout devices and magnetic tape recordings of signals, from the system sensors and electronic processing unit.

The test plan and the methods to be used in tabulating and analyzing the collected data shall be included as an appendix to the final report.

- 6. Testing Requirements:
- 7. Items to be Delivered:

None

The contractor shall submit the following written reports during performance of the work assignment.

- a. Monthly Letter Report
- b. Draft of Test Plan within two weeks after acceptance of work assignment.
- c. Final Proposed Test Plan within one week after approval of the draft plan.
- e. Final Work Assignment Report.

The Monthly Letter Reports and Final Work Assignment Report shall be prepared and distributed pursuant to instructions set forth in paragraph 4, Exhibit "A", Scope of Work, of basic contract.

8. Government Furnished Property and/or Assistance:

The Government will furnish the following reference materials to the contractor.

- a. Extracts from "Department of the Army Approved Small Development Requirement (SDR) for a Bullet Detection Device for Army Aircraft (U)," dated 22 October 1965, classified CONFIDENTIAL.
- b. LWL Draft Report, "An Airborne Acoustic Locator System," by J. Wenig and H. Forst, classified CONFIDENTIAL.
- c. Technical Report No. LWL-CR-08P3, "Acoustic Locator System (U)," dated September 1967, classified CONFIDENTIAL.

9. Estimated Cost:

The total cost of this work assignment is estimated to be \$8,000.00.

10. Estimated Completion Date:

Provided tests are not delayed, this work assignment will be completed within three (3) months after date of its acceptance by the contractor.

11. Technical Supervisor:

Joseph W. McMiell Chief, Research Analysis Branch USA Limited War Laboratory

Phone: Area Code 301, 278-4882

Alternate Technical Supervisor:

Donald O. Egner Research Analysis Branch USA Limited War Laboratory

Phone: Area Code 301, 278-4567

APPENDIX B

TEST OF THE IMPROVED ACOUSTIC LOCATORY SYSTEM ON THE COBRA (AH-1G) AIRCRAFT

APPENDIX B

TEST OF THE IMPROVED ACOUSTIC LOCATOR SYSTEMS ON THE COBRA (AH-1G) AIRCRAFT

Background: During mid 1968, it became apparent that the need for the Acoustic Locator System for the UH-1 aircraft had diminished since the Cobra aircraft had been introduced into Vietnam and the UH-1 was relegated to noncombat jobs and thus was exposed to less and less ground fire. The Cobra gun ship had become the major aircraft subject to ground fire.

Experimentation: Experimentation was performed to determine the best location for mounting the existing UH-1 type Acoustic Locator System on the Cobra aircraft. The pod of the Acoustic Locator System is the most critical element and must be mounted in such a position that smooth, non-turbulent airflow is obtained over the microphones. Various mounting locations on the Cobra were tried: (1) an outboard position, off the skids; (2) underneath the Cobra, behind the gun turret; and (3) a position on the nose of the aircraft. After noise measurements and "wool-tuft" (wind flow) tests, it was concluded that the nose mounting (shown in Figure B-1) was the least noisy and provided the smoothest airflow condition. From the data obtained, a noise match filter for the Cobra was inserted in the Acoustic Locatory System. The system, along with a tape recorder for recording signals, was mounted in the Cobra as shown in Figures B-2 and B-3.

Test Procedures: On 9 and 10 December 1968, acceptance tests, as discussed in Appendix A, were run on the Cobra-mounted Acoustic Locator System while flying the test course. On 16 December, several tests were run in which weapons systems mounted aboard the Cobra were fired. The weapons tested included the turret-mounted mini-gun, the turret-mounted 40mm grenade launcher, and the 2.7 wing-mounted rockets.

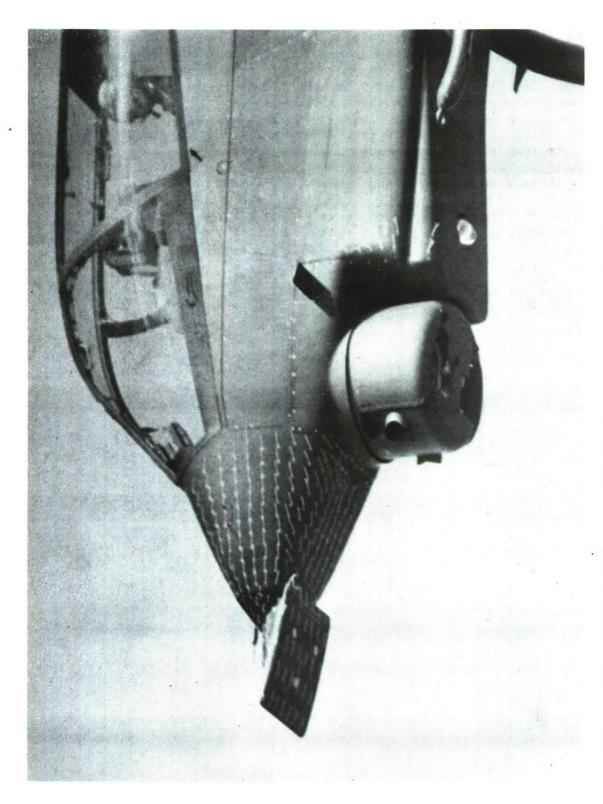
Results: The results of the acceptance tests using the M14 rifle are shown in Figure B-4 and Table B-1 and B-2. These indicate that the probability of detecting one or more signals is about as good for the Cobra as it is for the UH-1. However, the number of shots with an azimuth error less than 30° (this relates to the number of muzzle blasts detected and, hence, the location capability) is shown to be considerable less than was obtained in the UH-1. The false alarm rate for the system mounted on the Cobra was many times greater than that with the UH-1. Table B-3 tabulates the false alarm rates from the tape records for the Cobra. The UH-1 rate was so low that similar data was not obtained. This higher rate with the Cobra resulted from several causes: (1) the exposed mounting position of the pod which did not allow the body of the aircraft to shield the microphones from the downwash; (2) the increased wind noise resulting from the higher speeds possible in the Cobra aircraft; and (3) the greater incidence of rotor pop which comes from the combination of both the increased engine power and the exposure of the pod.

The firing of the turret-mounted weapons on the aircraft produced indications on the system which appeared toward the rear of the display (the proper direction as seen from the pod). As the weapons were swept, these indications moved in azimuth with the weapons. The mini-gun provided indications on just

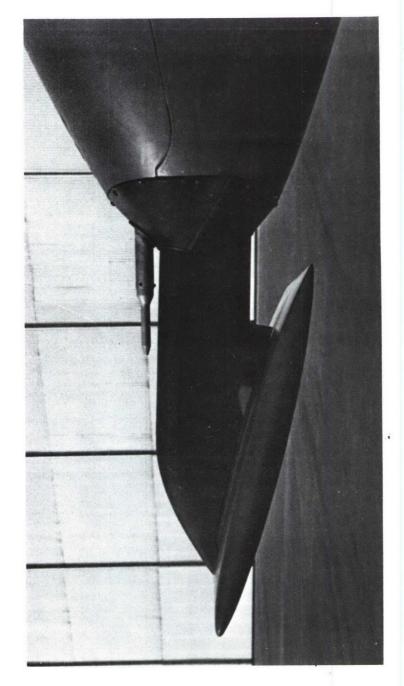
about every firing while the 40mm grenade launcher seldom gave signals. The firing of the wing-mounted rockets did not cause the Acoustic Locator System to display. The firing of the weapons, approximately two feet from the microphones, damaged one of the three microphones.

Upon examination by the manufacturer, it was concluded that the damage was not the type that should have resulted from overdriving the microphone accoustically. Thus, it is concluded that the microphones themselves were able to withstand these strong shock waves.

<u>Conclusion</u>: The high incidence of false alarms coupled with the low pointing-accuracy makes the present system unsuitable for use on the Cobra.



"Wool Tuft" tests with the Acoustic Locator System's pod mounted on the Cobra to monitor the air flow pattern. This picture was taken at 100 knots airspeed. Figure B-1.



The Acoustic Locator System's pod mounted on the nose of the Cobra. Figure B-2.

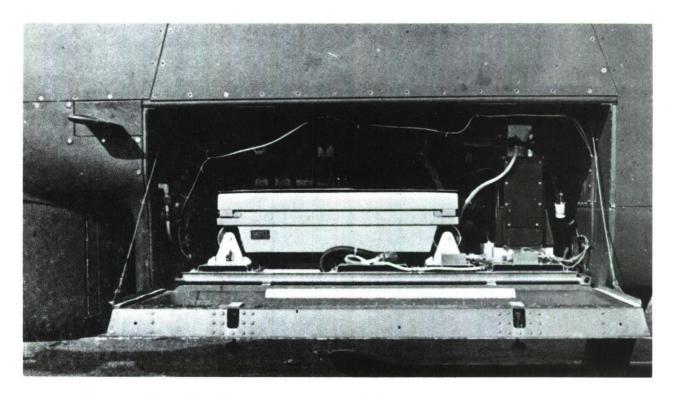
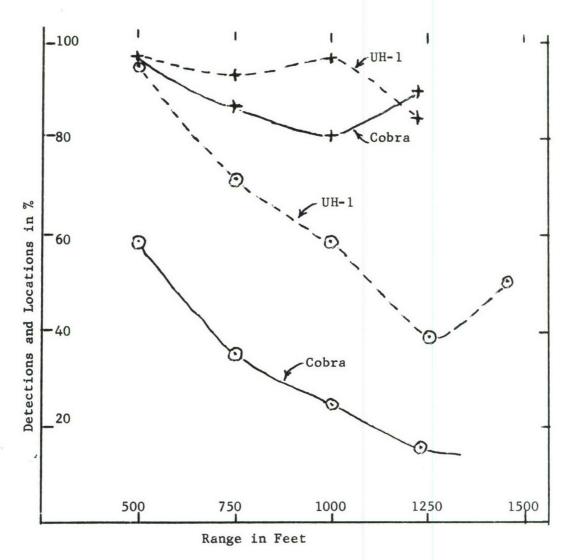


Figure B-3. The Electronics Box and data recorder mounted in the ammunition bay of the Cobra.



+ = Probability of Detecting one or more signals

Probability of correct locations (azimuth error less than 30°) All data is for the M-14 with a miss distance of 100 feet. The UH-1 data is from Appendix A, either Fig. 2 or Fig. 4.

Figure B-4. M-14 per cent detections and percent locations (azimuth error less than 30°) for the Acoustic Locator System on the Cobra and UH-1 aircrafts.

TABLE B-1. M-14, COBRA SUMMARY OF SIGNALS DETECTED

Number of Shots Displayed With:

Range	Zero Detection	1 Det.	2 Det.	3 or More Det.
500	1	5	14	12
750	4	7	13	7
1000	6	9	12	5
1200	3	7	16	5

See Appendix A, page 14 for similar UH-1 data

TABLE B-2. M-14, COBRA. MUZZLE BLAST SIGNALS RECEIVED

(i.e., those signals within 30° of their "should be" position in azimuth and greater than 40° elevation and two or more signals received)

Altitud	e Speed	Range		Received/Numbe	
50	20	500 2/4	750 1/3	0/4	2/4
50	20	2/4	1/3	0/4	2/4
50	80	3/4	2/4	0/4	1/3
50	120	2/4	2/4	1/4	0/4
50	160	1/4	1/4	0/4	0/4
200	20	4/4	3/4	1/4	0/4
200	80	4/4	1/4	3/4	1/4
200	120	2/2	1/4	2/4	1/4
200	160	1/4	0/4	1/4	0/4
Tota	1	19/32=.59	11/31=.35	8/32=.25	5/31=.16

See Appendix A, page 15 for similar UH-1 data

TABLE B-3. FALSE ALARM RATE, IN FALSE ALARMS PER SECOND, AS A FUNCTION OF THE PARAMETERS

Range	Attitude	Speed	False Alarm Rate	No. Sec. for Observation
	50	20	no data	
500'	50'	80	.05	40
	50	120	.31	190
	50	160	. 04	100
	200'	20	.083	120
	200	80	.01	100
	200	120	.01	100
	200	160	.012	78
750'	50	20	no data	
	50	80	no data	
	50	120	.26	57
	50	160	.01	102
	200	20	.088	90
	200	80	. 07	96
	200	120	.03	100
	200	160	.012	163
1000'	50	20	.08	104
	50	80	.03	106
	50	120	.01	103
	50	160	zero	66
	200'	20	.29	180
	200	80	.02	102
	200	120	.013	120
	200	160	zero	80
1200	50	20	.055	90
	50	80	.32	73
	50	120	.38	110
	50	160	. 03	160
	200	20	.167	72
	200	80	. 047	43
	200	120	.12	50
	200	160	no data	

Average rate = .098 false alarms/second

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